

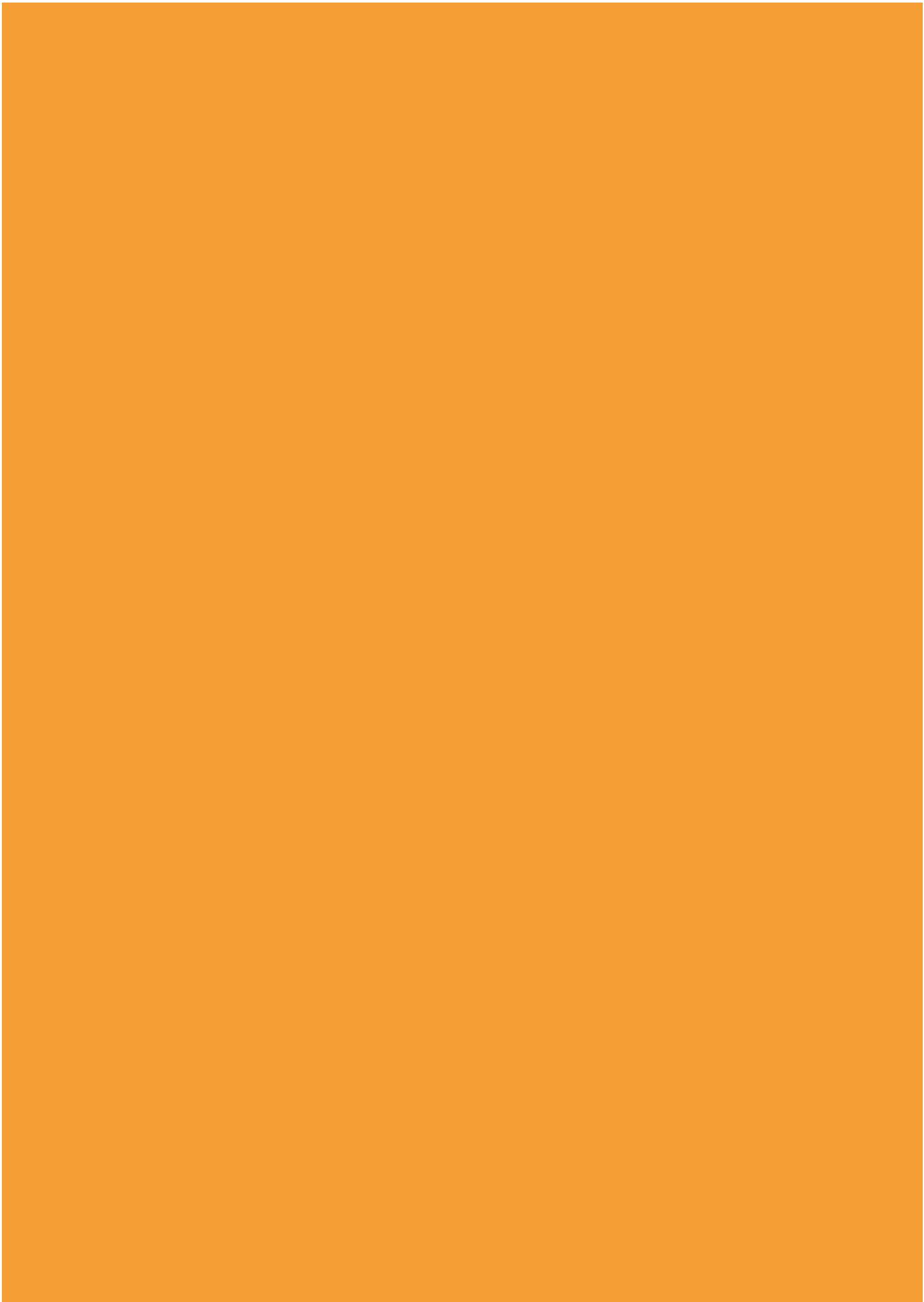
# | SILENT FLOOR PUR

## TECHNICAL MANUAL



rothoblaas

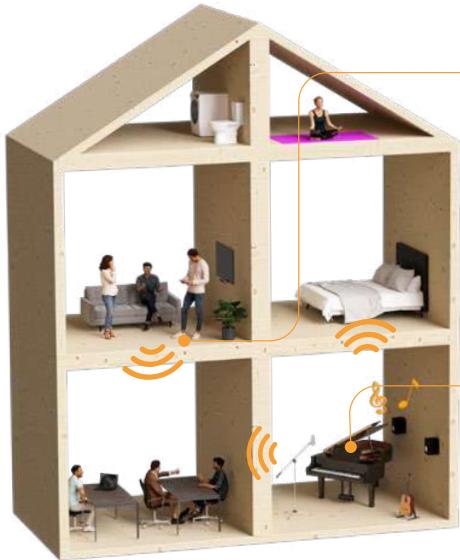
Solutions for Building Technology



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# ACOUSTIC PROBLEMS OF FLOORS



## WHAT IS IMPACT NOISE?

When it comes to floors, impact noise is the main acoustic problem because it constantly affects them. When a body impacts on the floor structure, the noise quickly spreads throughout the building either by air, affecting the nearest rooms, or by structure, propagating into the most distant rooms.



## WHAT IS AIRBORNE NOISE?

Airborne noise is generated in the air and, after an initial airborne phase, is transported both by air and by structure. This is a problem that affects both walls and floors, but if we are talking about floors, the most important problem is certainly impact noise.



## HERE IS THE SOLUTION

In order to be able to minimise the discomfort caused by impact noise, a stratigraphic package should be designed consisting of layers of different materials that are disconnected from each other and are able to dissipate the energy transmitted by the impact.



### MASS-SPRING-MASS SYSTEM

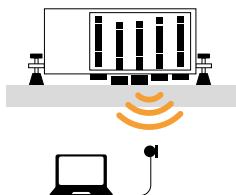
A floating screed system such as the one shown in the images below can be schematised with a mass-spring-mass system, in which the structural floor represents the mass, the impact-absorbing product is equivalent to the spring, and the upper screed with the floor constitutes the second mass of the system. In this context, "resilient layer" is defined as the element with the spring function characterised by its own *dynamic stiffness s'*.



## HOW IS THE IMPACT NOISE LEVEL MEASURED?

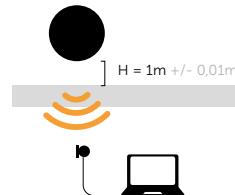
The impact noise level is a measure of the disturbance perceived in a room when an impact noise source is activated in the upper room. It can be measured both on site and in the laboratory. Clearly, ideal conditions exist in the laboratory for the effects of lateral transmission to be neglected, as the laboratory itself is constructed so that the walls are decoupled from the ceiling.

### TAPPING MACHINE method



The TAPPING MACHINE is used to simulate "light" and "hard" impacts, such as walking with heeled shoes or the impact caused by falling objects.

### RUBBER BALL method



The RUBBER BALL is used to simulate "soft" and "heavy" impacts, such as a barefoot walk or a child jumping.

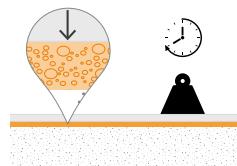
## ■ HOW TO CHOOSE THE BEST PRODUCT



### DYNAMIC STIFFNESS – $s'$

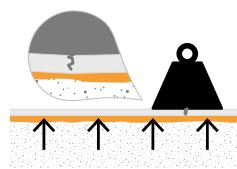
Expressed in MN/m<sup>3</sup>, it is measured according to EN 29052-1 and expresses the deformation capacity of a material that is subjected to a dynamic stress. Consequently, it indicates the ability to dampen the vibrations generated by an impact noise.

The measurement method involves, first, measuring the *apparent dynamic stiffness*  $s'_t$  of the material and then correcting it, if necessary, to obtain the *real dynamic stiffness*  $s'$ . Dynamic stiffness depends in fact on the flow resistivity  $r$ , which is measured in the lateral direction of the sample. If the material has specific flow resistivity values, the apparent dynamic stiffness must be corrected by adding the contribution of the gas contained within the material: air.



### VISCOS SLIDING UNDER COMPRESSION – CREEP

Expressed as a percentage, it is measured according to EN 1606 and represents the long-term deformation of a material under constant load to be simulated. The measurement in the laboratory must be carried out over a period of at least 90 days.

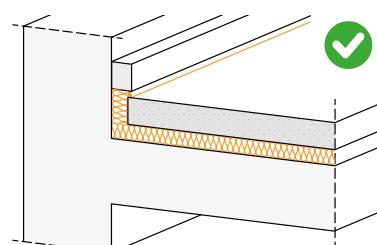
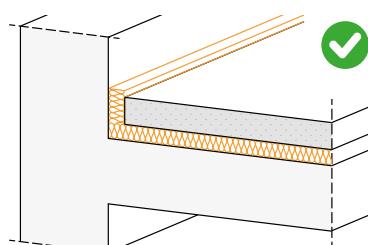
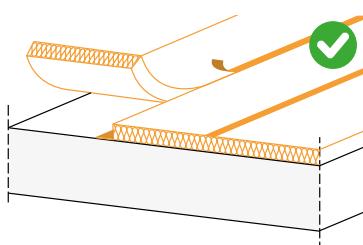
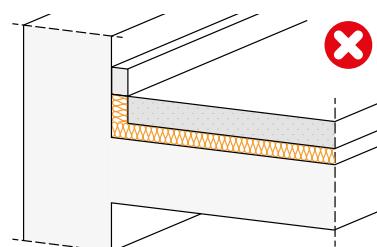
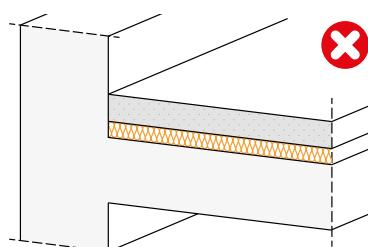
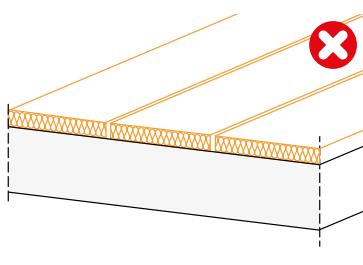


### COMPRESSIBILITY - c

The compressibility class expresses the behaviour of a material while subjected to screed loading. During measurement, the product is subjected to different loads and its thickness is measured. The compressibility measurement is carried out to understand what loads the underscreed product can withstand, in order to avoid cracking and splitting of screeds.

## ■ CORRECT INSTALLATION

The technological solution of the floating screed is one of the most widely used and one of the most effective, but in order to achieve satisfactory results it is important that the system is designed and implemented correctly.



The resilient layer must be continuous because any gap would represent an acoustic bridge. When installing underscreed mats, care must be taken not to create discontinuities.

It is important to use the SILENT EDGE perimeter strip to ensure that the resilient layer is continuous around the entire perimeter of the room. The SILENT EDGE should only be trimmed after the floor has been installed and grouted.

The skirting board must be installed after the SILENT EDGE has been cut, ensuring that it is always suitably raised from the floor.

## IIC vs L<sub>w</sub>

IIC stands for **Impact Insulation Class** and is the value obtained by subtracting the noise level measured in the receiving room from the noise level measured in the source room. Impact Insulation Class, sometimes referred to as Impact Isolation Class, measures the resistance of the floor construction assembly against the propagation of impact-generated noise.

# SILENT FLOOR PUR

RESILIENT HIGH PERFORMANCE UNDERSCREED MEMBRANE  
MADE OF RECYCLED POLYMERS

## CERTIFIED

The effectiveness of the underscreed membrane has been certified in the labs of the Centre for Industrial Research of the University of Bologna.

## SUSTAINABILITY

Recycled and recyclable. The product intelligently reuses polyurethane from production waste that would otherwise have to be disposed of.

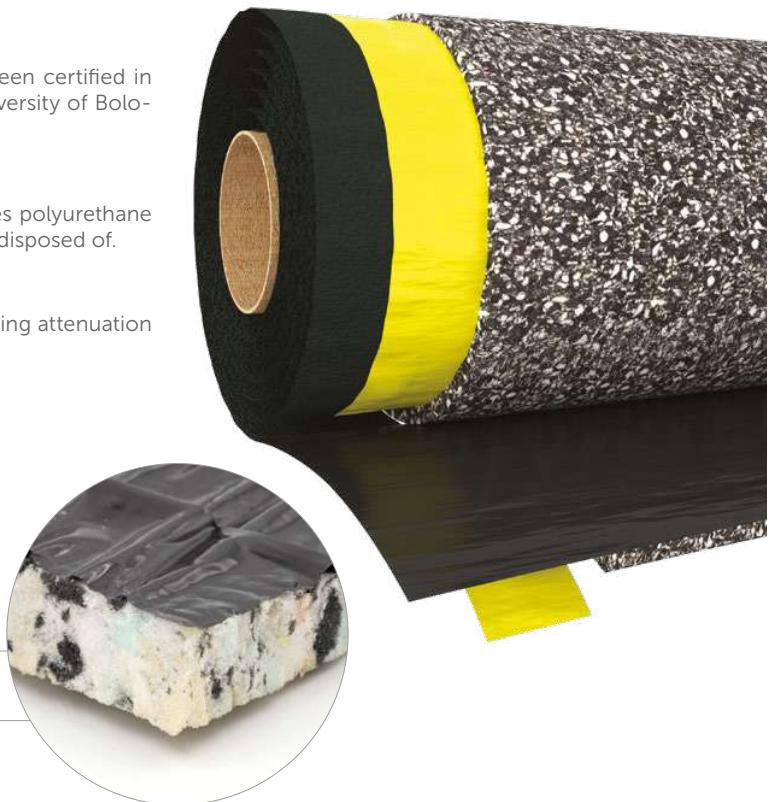
## HIGH PERFORMANCE

The special composition offers excellent elasticity, reaching attenuation values over 30 dB.

## COMPOSITION

polyethylene vapour barrier

polyurethane agglomerate made from pre-consumer industrial waste



## CODES AND DIMENSIONS

CODE	H <sup>(1)</sup> [m]	L [m]	thickness [mm]	A <sub>f</sub> <sup>(2)</sup> [m <sup>2</sup> ]	
SILFLOORPUR10	1,6	10	10	15	6
SILFLOORPUR15	1,6	8	15	12	6
SILFLOORPUR20	1,6	6	20	9	6

(1) 1.5 m of polyurethane agglomerate and vapour barrier + 0.1 m of vapour barrier for overlap with integrated adhesive strip.

(2) Without considering the overlap area.



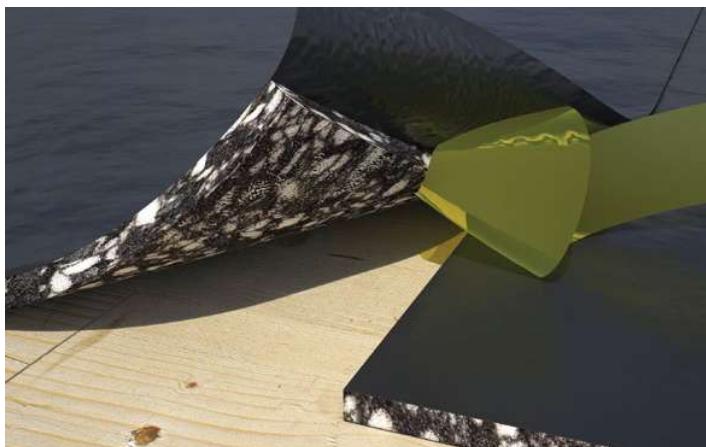
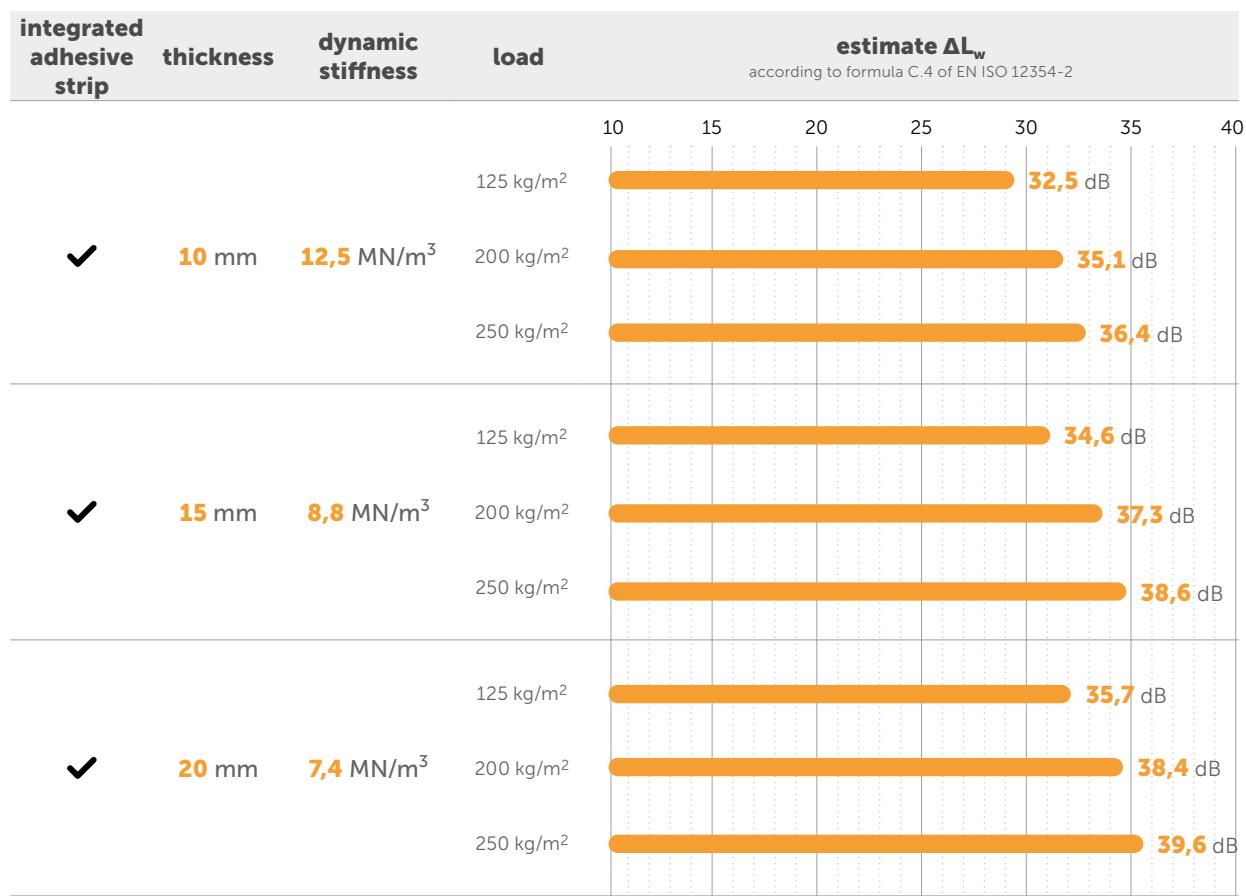
## SAFE

Polyurethane is a noble polymer that maintains elasticity over time, without subsidence or changes in performance.

## VOC REQUIREMENTS

The membrane composition safeguards health and meets the recommended VOC limits.

## ■ PRODUCT STRATIGRAPHY COMPARISON



# SILFLOORPUR10

## TECHNICAL DATA

Properties	standard	value
Surface mass m	-	0,9 kg/m <sup>2</sup>
Density ρ	-	80 kg/m <sup>3</sup>
Apparent dynamic stiffness s'	EN 29052-1	12,5 MN/m <sup>3</sup>
Dynamic stiffness s'	EN 29052-1	12,5 MN/m <sup>3</sup>
Theoretical estimate of impact sound pressure level attenuation ΔL <sub>w</sub> <sup>(1)</sup>	ISO 12354-2	32,5 dB
System resonance frequency f <sub>0</sub> <sup>(2)</sup>	ISO 12354-2	50,6 Hz
Impact sound pressure level attenuation ΔL <sub>w</sub> <sup>(3)</sup>	ISO 10140-3	21 dB
Thermal resistance R <sub>t</sub>	-	0,46 m <sup>2</sup> K/W
Resistance to airflow r	ISO 9053	< 10,0 kPa·s·m <sup>-2</sup>
Compressibility class	EN 12431	CP2
CREEP Viscous sliding under compression X <sub>ct</sub> (1,5 kPa)	EN 1606	7,50 %
Compression deformation stress	ISO 3386-1	17 kPa
Thermal conductivity λ	-	0,035 W/m·K
Specific heat c	-	1800 J/kg·K
Water vapour transmission Sd	-	> 100 m
Reaction to fire	EN 13501-1	class F
VOC emission classification	French decree no. 2011-321	A+

(1)  $\Delta L_w = (13 \lg(m')) - (14,2 \lg(s')) + 20,8$  [dB] con  $m' = 125$  kg/m<sup>2</sup>.

(2)  $f_0 = 160 \sqrt{s'/m'}$  con  $m' = 125$  kg/m<sup>2</sup>.

(3) Measured in the laboratory on 200 mm CLT floor. See the manual for more information on configuration.

## EN ISO 12354-2 ANNEX C | ESTIMATE ΔL<sub>w</sub> [FORMULA C.4] E ΔL [FORMULA C.1]

The following tables show how the attenuation in dB (ΔL<sub>w</sub> e ΔL) of SILFLOORPUR10 varies as the load m' (i.e., the surface mass of the layers with which SILFLOORPUR10 is loaded) changes.

SILFLOORPUR10

s' or s'	12,5	12,5	12,5	12,5	12,5	12,5	12,5	12,5	12,5	12,5	[MN/m <sup>3</sup> ]
load m'	50	75	100	125	150	175	200	225	250	275	[kg/m <sup>2</sup> ]
ΔL <sub>w</sub>	27,3	29,6	31,2	32,5	33,5	34,4	35,1	35,8	36,4	36,9	[dB]
f <sub>0</sub>	80,0	65,3	56,6	50,6	46,2	42,8	40,0	37,7	35,8	34,1	[Hz]

ΔL in frequency

[Hz]	<b>100</b>	2,9	5,5	7,4	8,9	10,1	11,1	11,9	12,7	13,4	14,0	14,6	[dB]
[Hz]	<b>125</b>	5,8	8,5	10,3	11,8	13,0	14,0	14,8	15,6	16,3	16,9	17,5	[dB]
[Hz]	<b>160</b>	9,0	11,7	13,5	15,0	16,2	17,2	18,1	18,8	19,5	20,1	20,7	[dB]
[Hz]	<b>200</b>	11,9	14,6	16,5	17,9	19,1	20,1	21,0	21,7	22,4	23,0	23,6	[dB]
[Hz]	<b>250</b>	14,8	17,5	19,4	20,8	22,0	23,0	23,9	24,6	25,3	26,0	26,5	[dB]
[Hz]	<b>315</b>	17,9	20,5	22,4	23,8	25,0	26,0	26,9	27,7	28,3	29,0	29,5	[dB]
[Hz]	<b>400</b>	21,0	23,6	25,5	26,9	28,1	29,1	30,0	30,8	31,5	32,1	32,6	[dB]
[Hz]	<b>500</b>	23,9	26,5	28,4	29,8	31,0	32,0	32,9	33,7	34,4	35,0	35,5	[dB]
[Hz]	<b>630</b>	26,9	29,5	31,4	32,9	34,0	35,0	35,9	36,7	37,4	38,0	38,6	[dB]
[Hz]	<b>800</b>	30,0	32,6	34,5	36,0	37,2	38,2	39,0	39,8	40,5	41,1	41,7	[dB]
[Hz]	<b>1000</b>	32,9	35,5	37,4	38,9	40,1	41,1	41,9	42,7	43,4	44,0	44,6	[dB]
[Hz]	<b>1250</b>	35,8	38,5	40,3	41,8	43,0	44,0	44,8	45,6	46,3	46,9	47,5	[dB]
[Hz]	<b>1600</b>	39,0	41,7	43,5	45,0	46,2	47,2	48,1	48,8	49,5	50,1	50,7	[dB]
[Hz]	<b>2000</b>	41,9	44,6	46,5	47,9	49,1	50,1	51,0	51,7	52,4	53,0	53,6	[dB]
[Hz]	<b>2500</b>	44,8	47,5	49,4	50,8	52,0	53,0	53,9	54,6	55,3	56,0	56,5	[dB]
[Hz]	<b>3150</b>	47,9	50,5	52,4	53,8	55,0	56,0	56,9	57,7	58,3	59,0	59,5	[dB]

EN ISO 12354-2 Annex C - formula C.4

$$\square \quad \Delta L_w = \left( 13 \lg(m') \right) - \left( 14,2 \lg(s') \right) + 20,8 \text{ dB}$$

EN ISO 12354-2 Annex C - formula C.1

$$\square \quad \Delta L = \left( 30 \lg \frac{f}{f_0} \right) \text{dB}$$

EN ISO 12354-2 Annex C - formula C.2

$$\square \quad f_0 = 160 \sqrt{\frac{s'}{m'}}$$

# IMPACT NOISE INSULATION ACCORDING TO SCREED THICKNESS

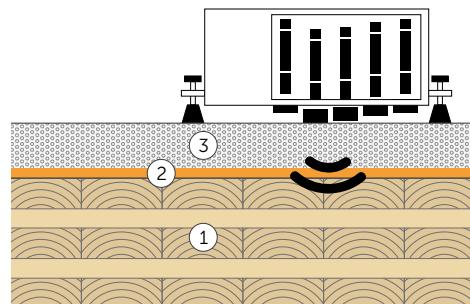
A predictive study of the sound insulation of airborne and impact noise in buildings cannot be determined by calculations alone, but must be supported by experimental data and measurements in the laboratory and on site.

The acoustics laboratory at the University of Northern British Columbia is designed optimized for testing the sound insulation performance of floors in timber buildings. In fact, the receiving room is built of frame walls made of mullions and interposed rock wool insulation and OSB sheathing and two layers of gypsum board.

Impact noise assessment is measured according to ASTM E1007-15 using the impact sound machine and a sound pressure meter according to ISO. The tests involve evaluating the acoustic behavior of the floor slab according to the thickness of the screed (38 mm, 50 mm, 100 mm).

## MATERIALS

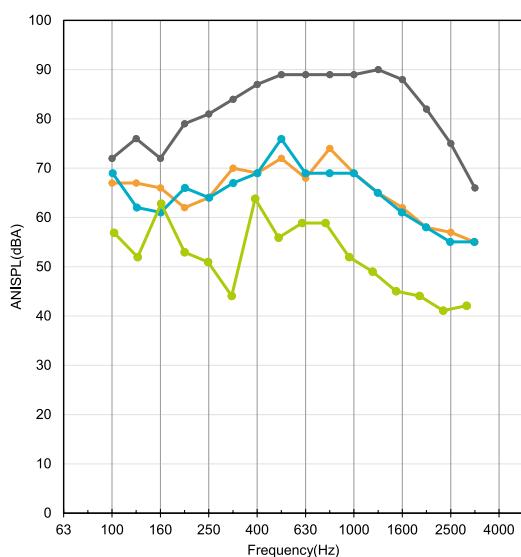
- ① **X-LAM FLOOR SLABS:** The tested floor slab consists of three of 139 mm thick CLT 139V panels. Each CLT panel is 4.0 m long and 1.8 m wide. All joints are sealed with acoustic sealant and tapes. The edges between floors and walls are also sealed with acoustic sealant. The AIIC of the bare CLT floor slab is 21 ( $L'_{n,w} = 89\text{dB}$ )
- ② **SILENT FLOOR PUR:** high-performance resilient agglomerate underscreed membrane made from pre-consumer industrial waste and PE vapour barrier.
- ③ **Screeds:** ordinary concrete
  - thickness 38 mm,  $91 \text{ kg/m}^2$
  - thickness 50 mm,  $120 \text{ kg/m}^2$
  - thickness 100 mm,  $240 \text{ kg/m}^2$



## RESULTS

- CLT
- CLT + SILENT FLOOR PUR + 38 mm concrete
- CLT + SILENT FLOOR PUR + 50 mm concrete
- CLT + SILENT FLOOR PUR + 100 mm concrete

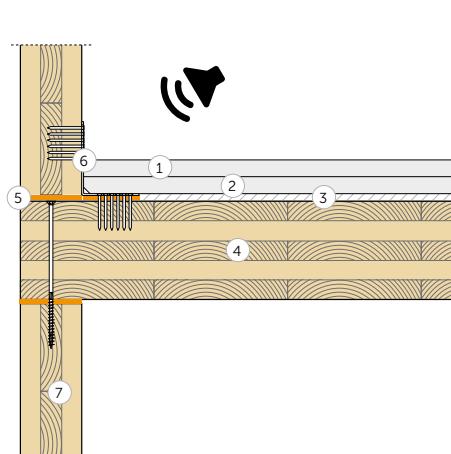
	AIIC (dBA)	$L'_{n,w}$ (dB)	Acoustic improvement (dB)
— CLT	21	89	
— CLT + SILENT FLOOR PUR + 38 mm concrete	41	69	<b>20</b>
— CLT + SILENT FLOOR PUR + 50 mm concrete	42	68	<b>21</b>
— CLT + SILENT FLOOR PUR + 100 mm concrete	48	62	<b>27</b>



Testing laboratory: University of Northern British Columbia  
Test protocol: 20200720

## ■ LABORATORY MEASUREMENT | CLT FLOOR 1

AIRBORNE SOUND INSULATION ACCORDING TO ISO 16283-1



### FLOOR SLAB

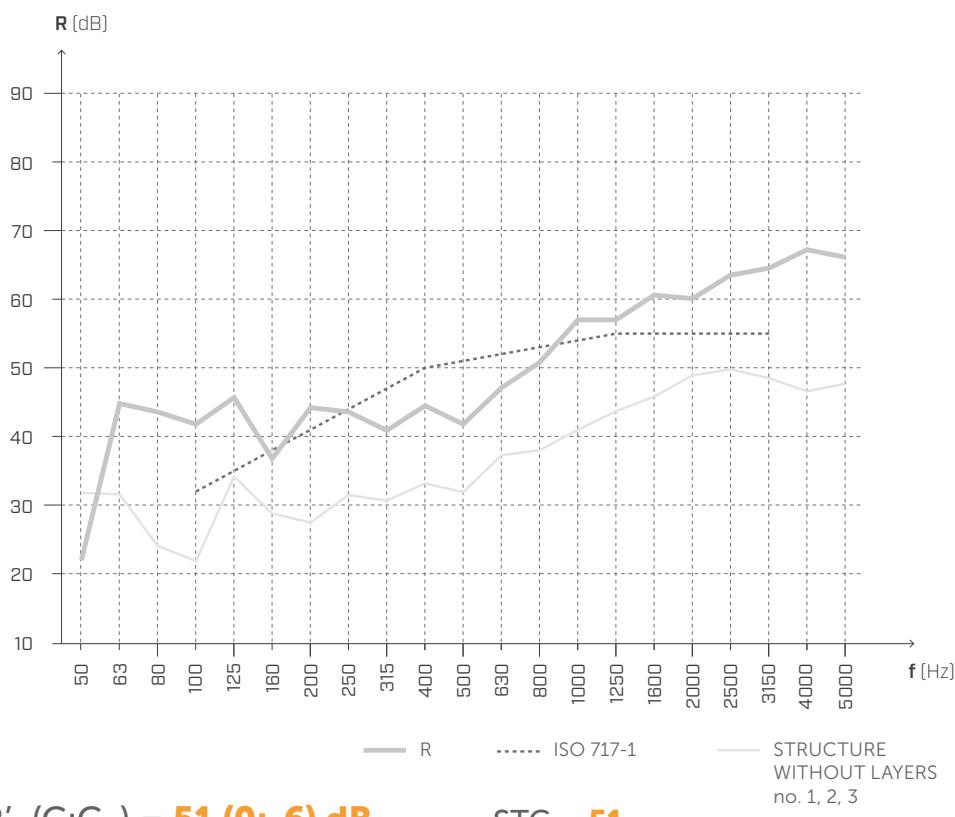
Surface = 21,64 m<sup>2</sup>

Mass = 167 kg/m<sup>2</sup>

Receiving room volume = 75,52 m<sup>3</sup>

- ① Reinforced gypsum-fibre board (44 kg/m<sup>2</sup>) (thickness: 32 mm)
- ② High density cardboard and sand panels (34,6 kg/m<sup>2</sup>) (thickness: 30 mm)
- ③ SILENT FLOOR PUR - SILFLOORPUR10 (thickness: 10 mm)
- ④ CLT (thickness: 160 mm)
- ⑤ XYLOFON 35 - XYL35100
- ⑥ TITAN SILENT
- ⑦ CLT (thickness: 120 mm)

## ■ AIRBORNE SOUND INSULATION



$$R'_w(C; C_{tr}) = \mathbf{51 (0;-6) dB}$$

$$\Delta R'_w = +12 dB^{(1)}$$

$$STC = \mathbf{51}$$

$$\Delta STC = +12^{(1)}$$

Testing laboratory: Universität Innsbruck Arbeitsbereich für Holzbau  
Technikerstraße 13A - 6020 Innsbruck.

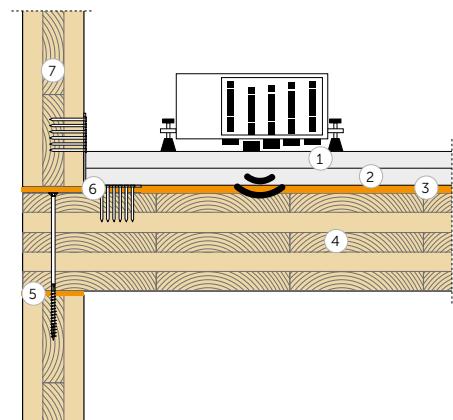
Test protocol: M07B\_L211217\_m-Bodenaufbau

### NOTES:

<sup>(1)</sup> Increase due to the addition of layers no. 1, 2 and 3.

## LABORATORY MEASUREMENT | CLT FLOOR 1

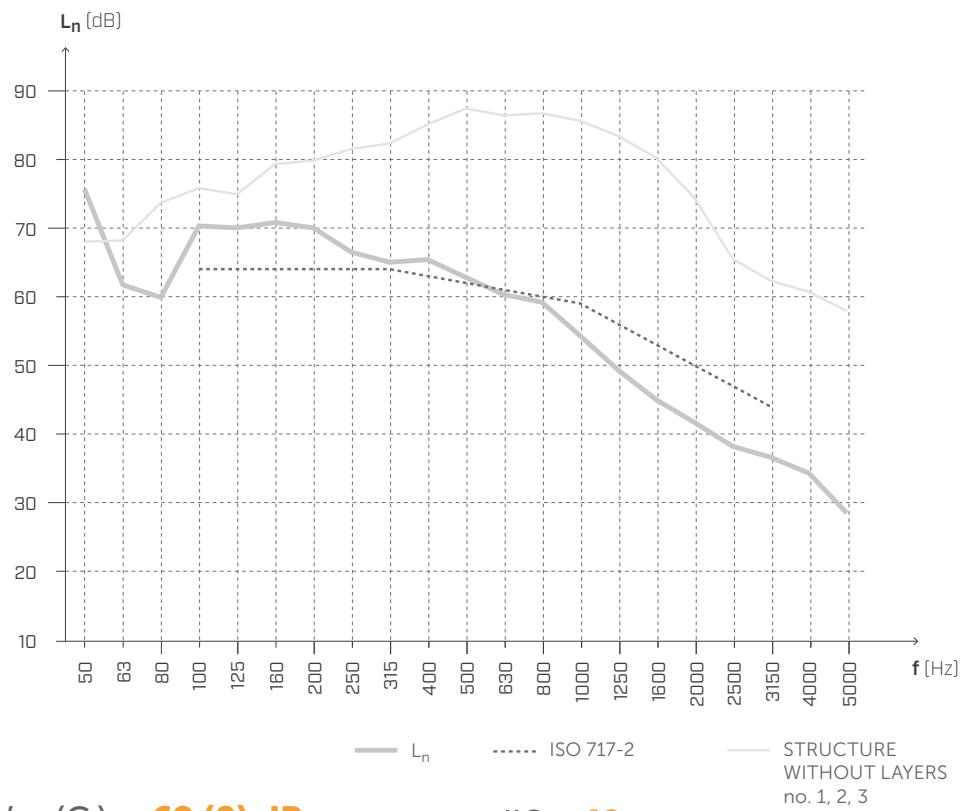
IMPACT SOUND INSULATION ACCORDING TO ISO 16283-1



**Surface** = 21,64 m<sup>2</sup>  
**Mass** = 167 kg/m<sup>2</sup>  
**Receiving room volume** = 75,52 m<sup>3</sup>

- ① Reinforced gypsum-fibre board (44 kg/m<sup>2</sup>) (thickness: 32 mm)
- ② high density cardboard and sand panels (34,6 kg/m<sup>2</sup>), (thickness: 30 mm)
- ③ **SILENT FLOOR PUR- SILFLOORPUR10** (s: 10 mm)
- ④ CLT (thickness: 160 mm)
- ⑤ **XYLOFON 35 - XYL35100**
- ⑥ TITAN SILENT
- ⑦ CLT (thickness: 120 mm)

### Impact sound NOISE INSULATION



$$L'_{n,w}(C_l) = 62 \text{ (0)} \text{ dB}$$

$$\Delta L_{n,w}(C_l) = -22 \text{ dB}^{(1)}$$

$$IIC = 48$$

$$\Delta IIC = +22^{(2)}$$

**Testing laboratory:** Universität Innsbruck Arbeitsbereich für Holzbau  
 Technikerstraße 13A - 6020 Innsbruck.

**Test protocol:** M07B\_T211217\_m-Bodenaufbau

#### NOTES:

<sup>(1)</sup> Decrease due to the addition of layers no. 1 and no. 2.

<sup>(2)</sup> Increase due to the addition of layers no. 1 and no. 2.

## LABORATORY MEASUREMENT | CLT FLOOR 2

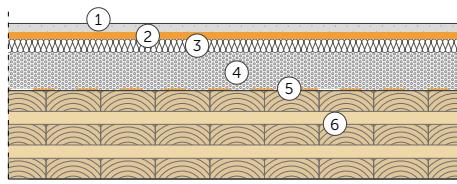
MEASUREMENT OF AIRBORNE SOUND INSULATION EVALUATION INDEX  
REFERENCE STANDARD ISO 10140-2

### FLOOR SLAB

Surface = 12 m<sup>2</sup>

Mass = 230 kg/m<sup>2</sup>

Receiving room volume = 54,7 m<sup>3</sup>



① Concrete screed (2000 kg/m<sup>3</sup>) (thickness: 50 mm)

② **SILENT FLOOR PUR** (thickness: 10 mm)

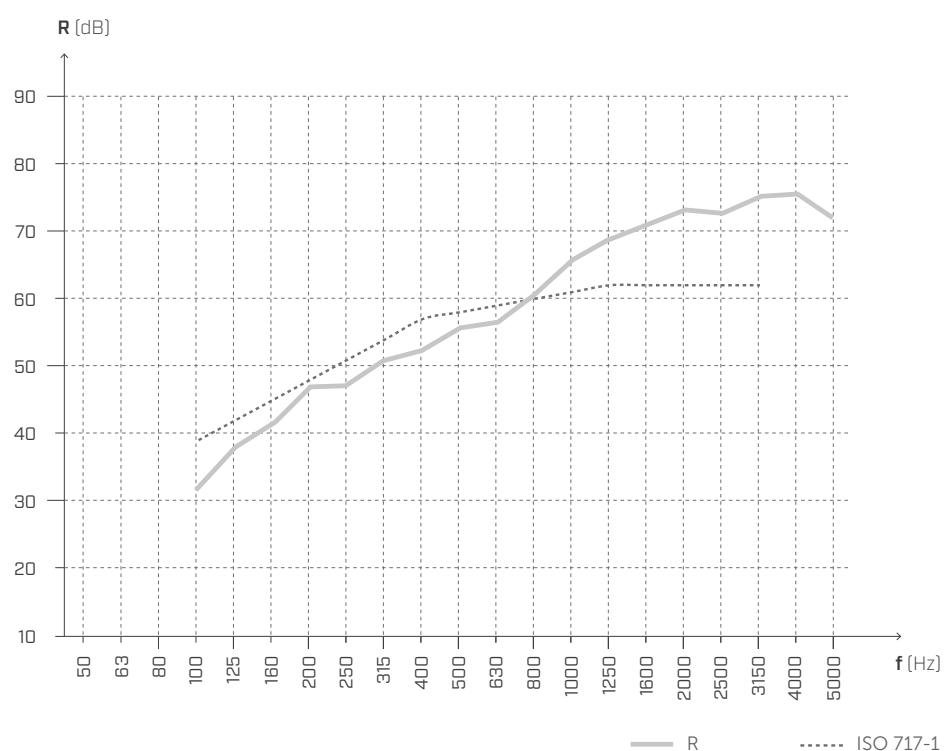
③ Mineral wool insulation s' ≤ 10 MN/m<sup>3</sup> (110 kg/m<sup>3</sup>) (thickness 40 mm)

④ Light screed with EPS (500 kg/m<sup>3</sup>) (thickness: 120 mm)

⑤ **BARRIER SD150**

⑥ CLT 5 layers (thickness: 150 mm)

## AIRBORNE SOUND INSULATION



$$R_w = \mathbf{57 \, (-2;-9) \, dB}$$

$$STC = \mathbf{57}$$

Testing laboratory: Alma Mater Studiorum Università di Bologna  
Test protocol: 01L/RothoB

## LABORATORY MEASUREMENT | CLT FLOOR 2

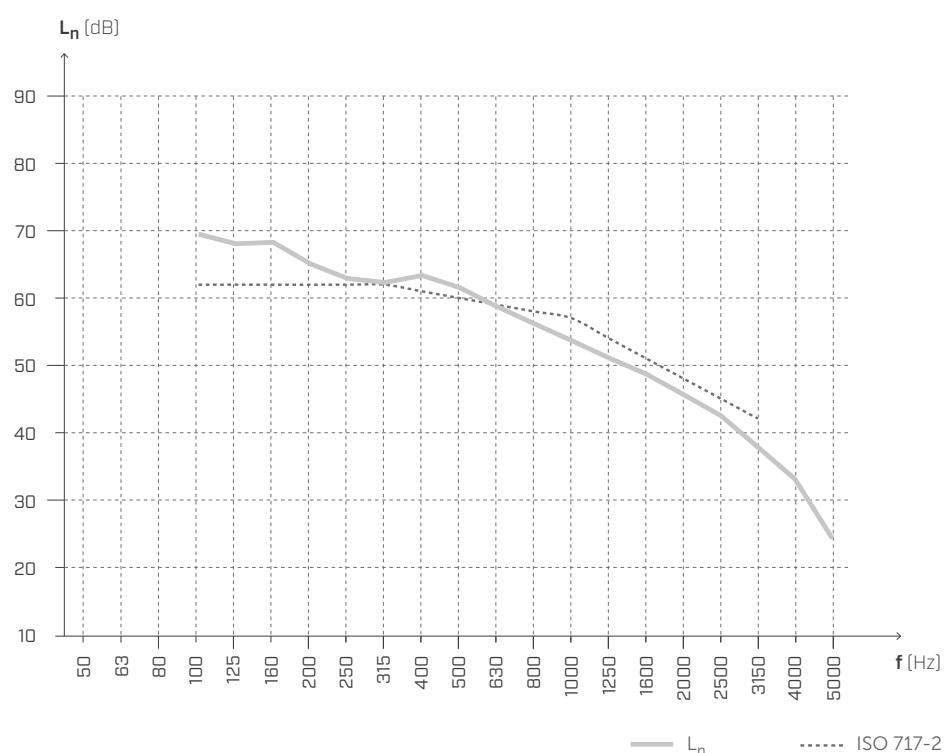
MEASUREMENT OF THE EVALUATION INDEX OF THE REDUCTION OF THE IMPACT SOUND PRESSURE LEVEL  
REFERENCE STANDARD: ISO 10140-3 AND EN ISO 717-2

### FLOOR SLAB

Surface = 12 m<sup>2</sup>  
Mass = 230 kg/m<sup>2</sup>  
Receiving room volume = 54,7 m<sup>3</sup>



## IMPACT SOUND INSULATION



$$L_{n,w}(C_l) = 60(0) \text{ dB}$$

$$\Delta L_{n,w}(C_l) = -27 \text{ dB}^{(1)}$$

$$IIC = 50$$

$$\Delta IIC = +27^{(2)}$$

Testing laboratory: Alma Mater Studiorum Università di Bologna  
Test protocol: 01R/RothoB

### NOTES:

<sup>(1)</sup> Decrease due to the addition of layers no. 1 and no. 2.

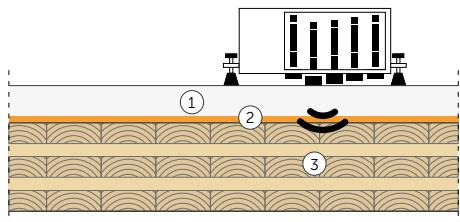
<sup>(2)</sup> Increase due to the addition of layers no. 1 and no. 2.

## LABORATORY MEASUREMENT | CLT FLOOR 3

MEASUREMENT OF THE EVALUATION INDEX OF THE REDUCTION OF THE IMPACT SOUND PRESSURE LEVEL  
REFERENCE STANDARD: ISO 10140-3 AND EN ISO 717-2

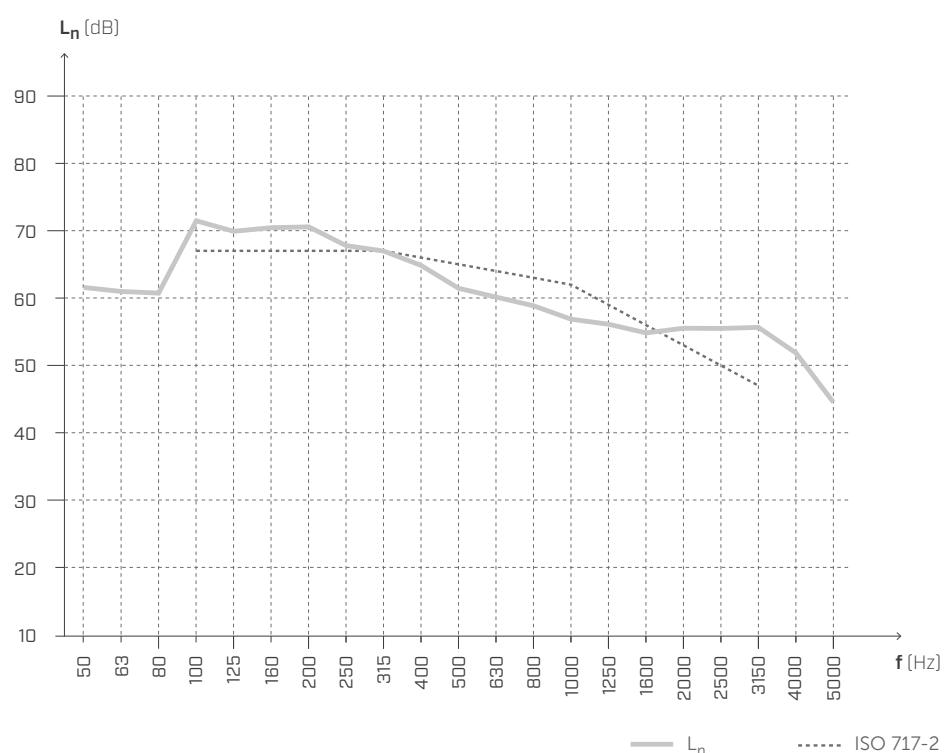
### FLOOR SLAB

Surface = 13,71 m<sup>2</sup>  
Surface mass = 215,1 kg/m<sup>2</sup>  
Receiving room volume = 60,1 m<sup>3</sup>



- ① Concrete screed (thickness: 50 mm); (2600 kg/m<sup>3</sup>); (130 kg/m<sup>2</sup>)
- ② **SILENT FLOOR PUR - SILFLOORPUR10** (thickness: 10 mm)
- ③ CLT 5 layers (thickness: 200 mm); (420 kg/m<sup>3</sup>); (84 kg/m<sup>2</sup>)

## IMPACT SOUND INSULATION



$$L_{n,w}(C_l) = \mathbf{65 (-2) dB}$$

$$\Delta L_{n,w}(C_l) = -21 dB^{(1)}$$

$$IIC = \mathbf{44}$$

$$\Delta IIC = +20^{(2)}$$

Testing laboratory: Building Physics Lab | Libera Università di Bolzano.

Test protocol: Pr. 2022-rothoLATE-L2.

### NOTES:

<sup>(1)</sup> Decrease due to the addition of layers no. 1 and no. 2.

<sup>(2)</sup> Increase due to the addition of layers no. 1 and no. 2.

## ■ LABORATORY MEASUREMENT | CLT FLOOR 3

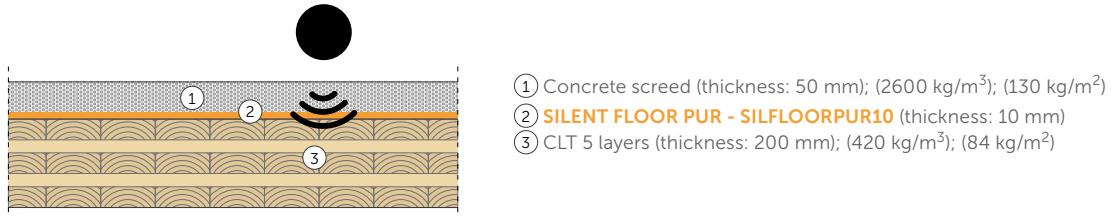
MEASUREMENT OF THE EVALUATION INDEX OF THE REDUCTION OF THE IMPACT SOUND PRESSURE LEVEL  
RUBBER BALL METHOD | REFERENCE STANDARD: ISO 10140-3 AND EN ISO 717-2

### FLOOR SLAB

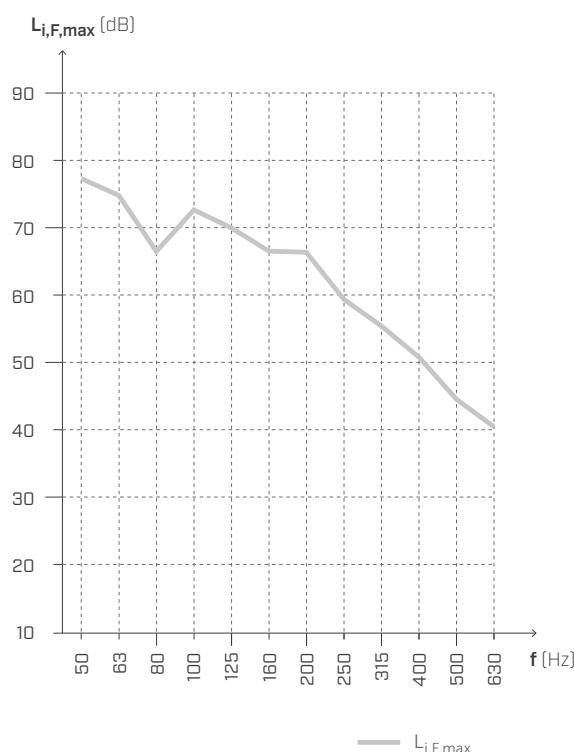
Surface = 13,71 m<sup>2</sup>

Surface mass = 215,1 kg/m<sup>2</sup>

Receiving room volume = 60,1 m<sup>3</sup>



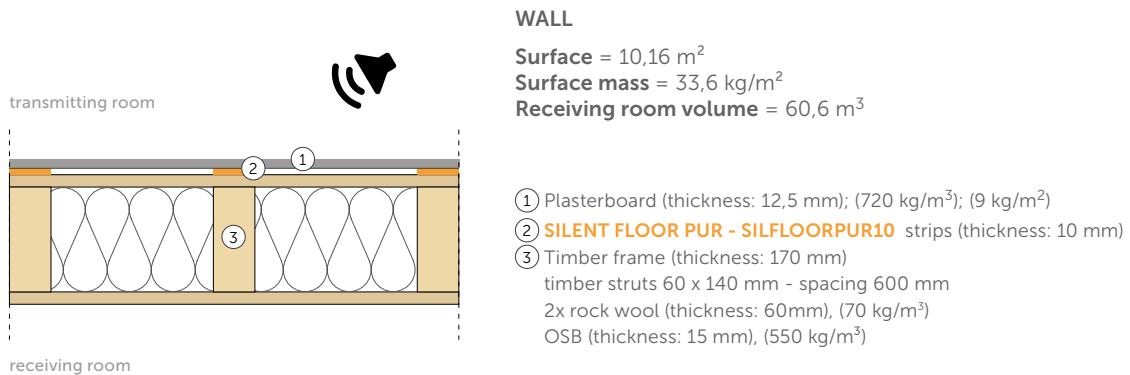
## ■ IMPACT SOUND INSULATION



Testing laboratory: Building Physics Lab | Libera Università di Bolzano.  
Test protocol: Pr. 2022-rothoLATE-L2.

## ■ LABORATORY MEASUREMENT | FRAME WALL 4A

MEASUREMENT OF AIRBORNE SOUND INSULATION EVALUATION INDEX  
REFERENCE STANDARD: ISO 10140-2 AND EN ISO 717-1



## ■ AIRBORNE SOUND INSULATION



$$R_w(C, C_{tr}) = \mathbf{47} \text{ (-2;-8) dB}$$

$$STC = \mathbf{48}$$

$$\Delta R_w = +6 \text{ dB}^{(1)}$$

$$\Delta STC = +7 \text{ dB}^{(1)}$$

**Testing laboratory:** Building Physics Lab | Libera Università di Bolzano.

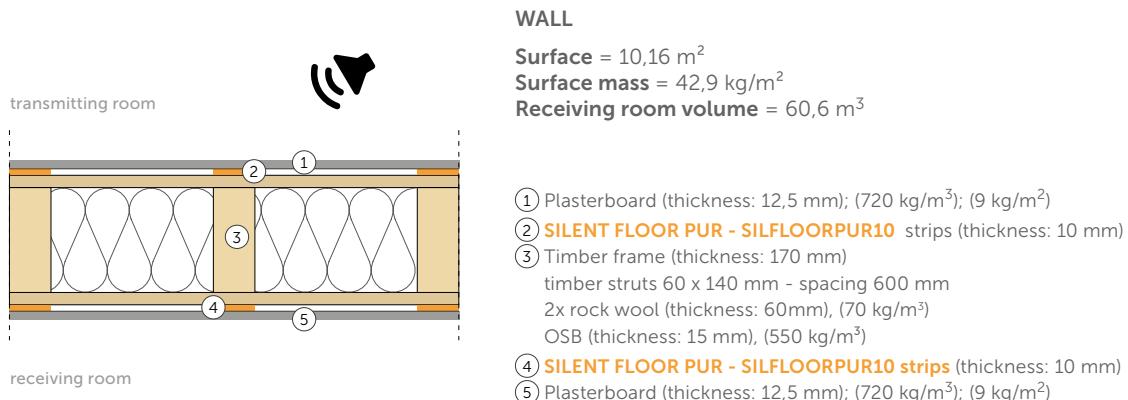
**Test protocol:** Pr. 2022-rothoLATE-R6a.

**NOTES:**

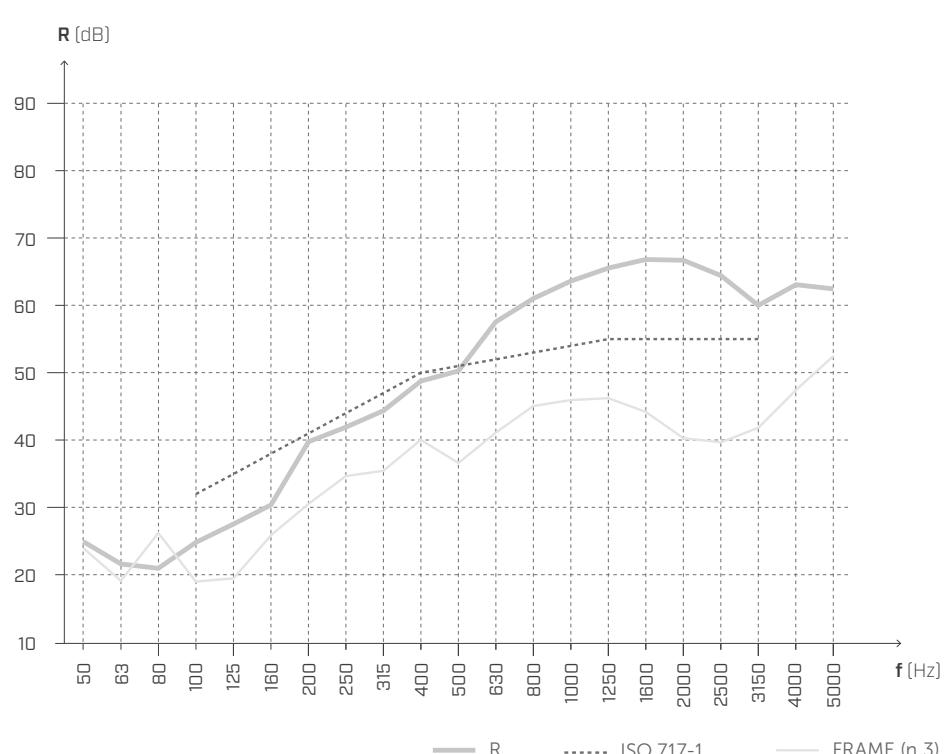
<sup>(1)</sup> Increase due to the addition of layers no. 1 and no. 2.

## LABORATORY MEASUREMENT | CLT FLOOR 4B

MEASUREMENT OF AIRBORNE SOUND INSULATION EVALUATION INDEX  
REFERENCE STANDARD: ISO 10140-2 AND EN ISO 717-1



## AIRBORNE SOUND INSULATION



$$R_w(C; C_{tr}) = 51 \text{ (-3;-10) dB}$$

$$\Delta R_w = +10 \text{ dB}^{(1)}$$

$$STC = 51$$

$$\Delta STC = +10^{(1)}$$

**Testing laboratory:** Building Physics Lab | Libera Università di Bolzano.

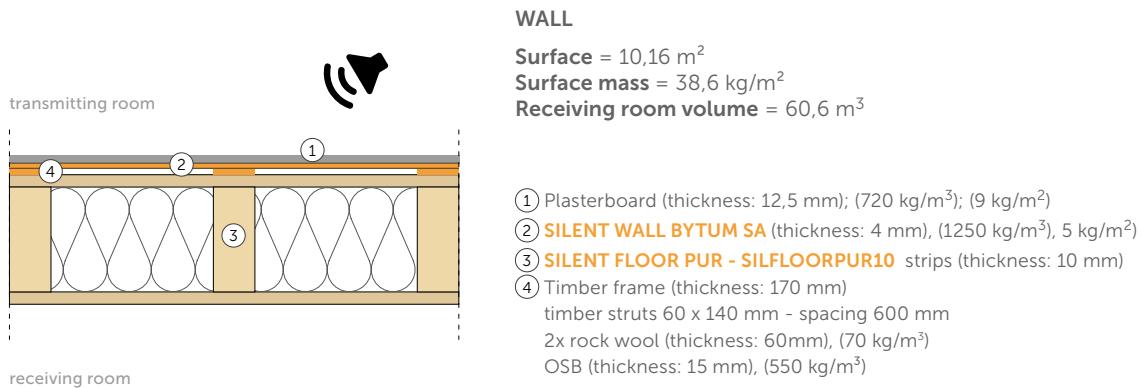
**Test protocol:** Pr. 2022-rothoLATE-R6b.

**NOTES:**

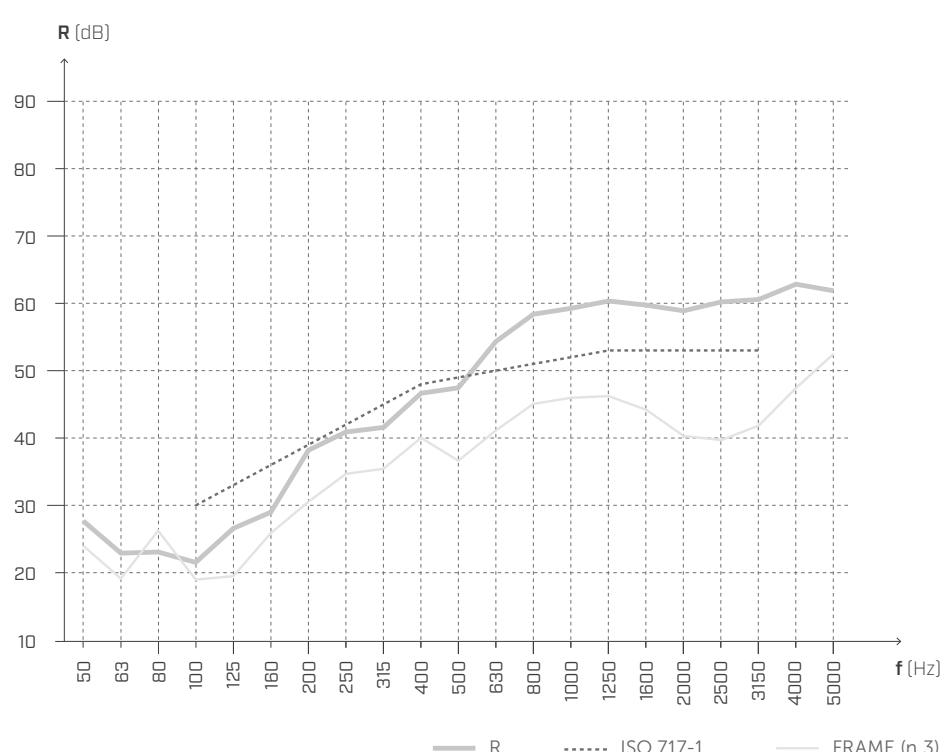
<sup>(1)</sup> Increase due to the addition of layers no. 1 and no. 2.

## LABORATORY MEASUREMENT | FRAME WALL 5A

MEASUREMENT OF AIRBORNE SOUND INSULATION EVALUATION INDEX  
REFERENCE STANDARD: ISO 10140-2 AND EN ISO 717-1



## AIRBORNE SOUND INSULATION



$$R_w(C, C_{tr}) = 49 \text{ (-3;-10) dB}$$

$$\Delta R_w = +8 \text{ dB}^{(1)}$$

$$\Delta STC = +9^{(1)}$$

**Testing laboratory:** Building Physics Lab | Libera Università di Bolzano.

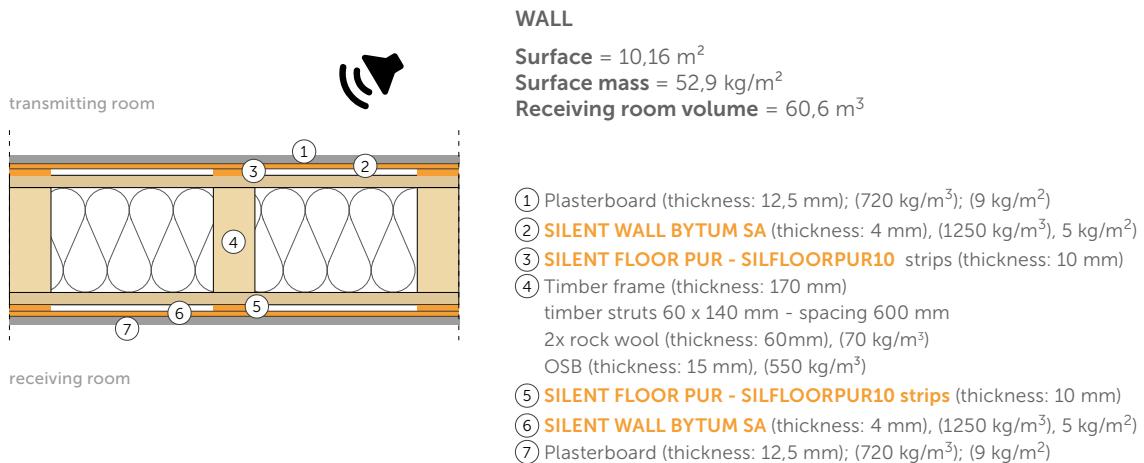
**Test protocol:** Pr. 2022-rothoLATE-R5a.

### NOTES:

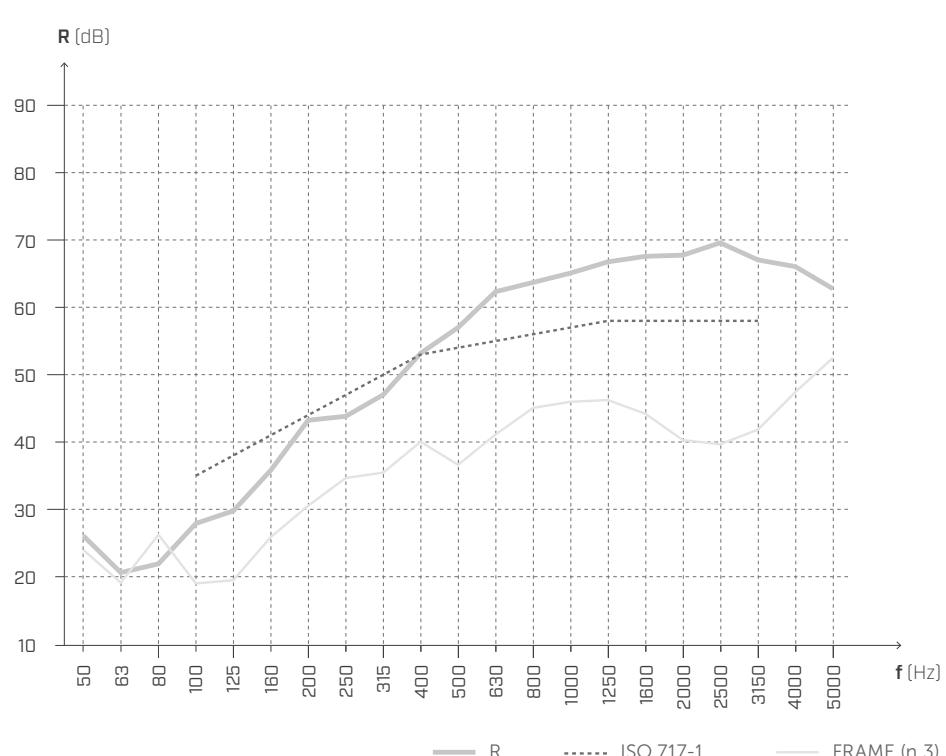
<sup>(1)</sup> Increase due to the addition of layers no. 1 and no. 2.

## LABORATORY MEASUREMENT | FRAME WALL 5B

MEASUREMENT OF AIRBORNE SOUND INSULATION EVALUATION INDEX  
REFERENCE STANDARD: ISO 10140-2 AND EN ISO 717-1



## AIRBORNE SOUND INSULATION



$$R_w(C, C_{tr}) = \mathbf{54} \text{ (-3;-9) dB}$$

$$\Delta R_w = +13 \text{ dB}^{(1)}$$

$$STC = \mathbf{54}$$

$$\Delta STC = +13 \text{ dB}^{(1)}$$

**Testing laboratory:** Building Physics Lab | Libera Università di Bolzano.

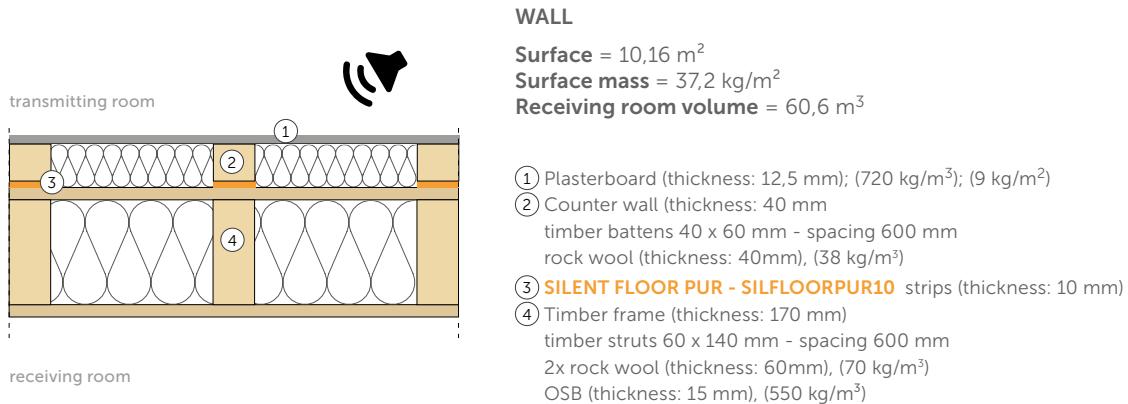
**Test protocol:** Pr. 2022-rothoLATE-R5b.

**NOTES:**

<sup>(1)</sup> Increase due to the addition of layers no. 1 and no. 2.

## LABORATORY MEASUREMENT | FRAME WALL 6A

MEASUREMENT OF AIRBORNE SOUND INSULATION EVALUATION INDEX  
REFERENCE STANDARD: ISO 10140-2 AND EN ISO 717-1



## AIRBORNE SOUND INSULATION



$$R_w(C, C_{tr}) = \mathbf{50} \text{ (-4;-10) dB}$$

$$\Delta R_w = +9 \text{ dB}^{(1)}$$

$$STC = \mathbf{48}$$

$$\Delta STC = +7^{(1)}$$

**Testing laboratory:** Building Physics Lab | Libera Università di Bolzano.

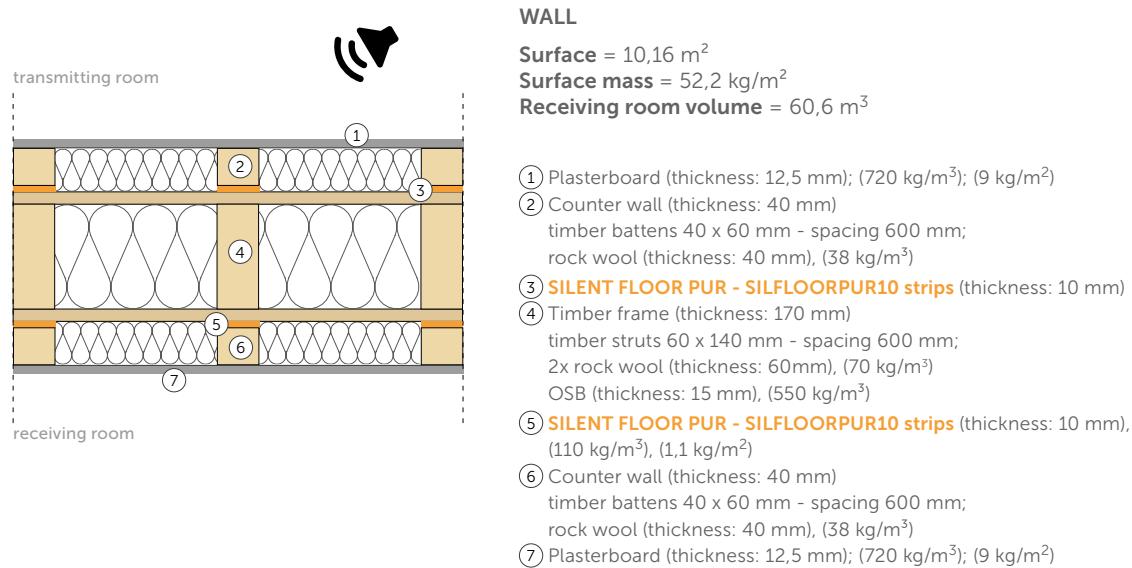
**Test protocol:** Pr. 2022-rothoLATE-R12a.

**NOTES:**

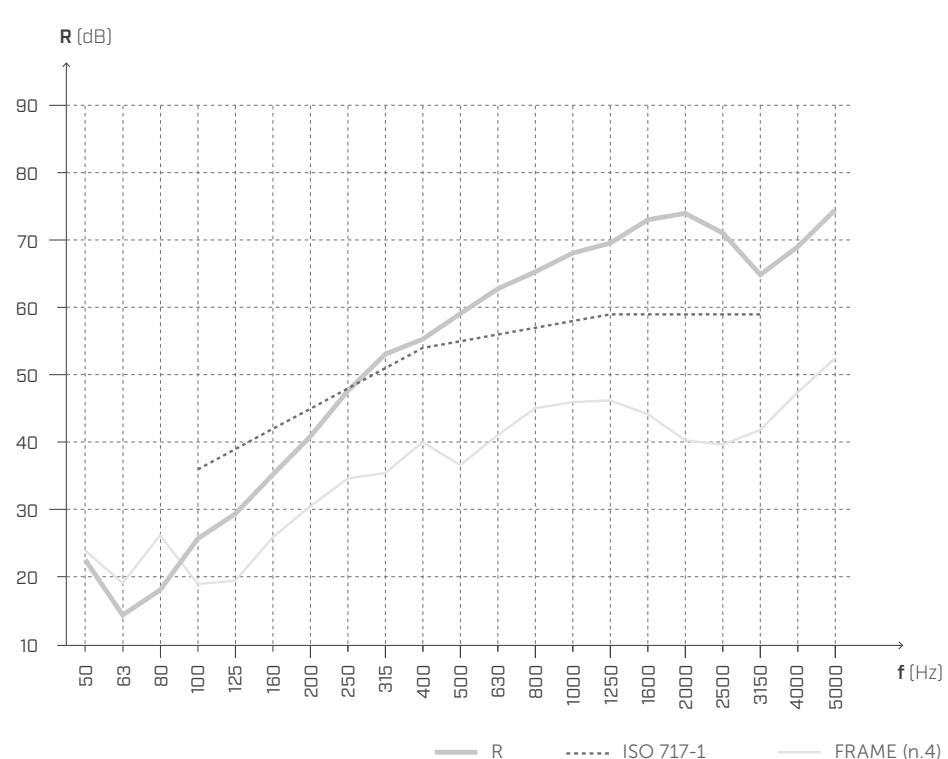
<sup>(1)</sup> Increase due to the addition of layers no. 1 and no. 2.

## LABORATORY MEASUREMENT | FRAME WALL 6B

MEASUREMENT OF AIRBORNE SOUND INSULATION EVALUATION INDEX  
REFERENCE STANDARD ISO 10140-2



## AIRBORNE SOUND INSULATION



$$R_w(C, C_{tr}) = 55 \text{ (-5;-12) dB}$$

$$\Delta R_w = +14 \text{ dB}^{(1)}$$

$$STC = 53$$

$$\Delta STC = +12^{(1)}$$

**Testing laboratory:** Building Physics Lab | Libera Università di Bolzano.

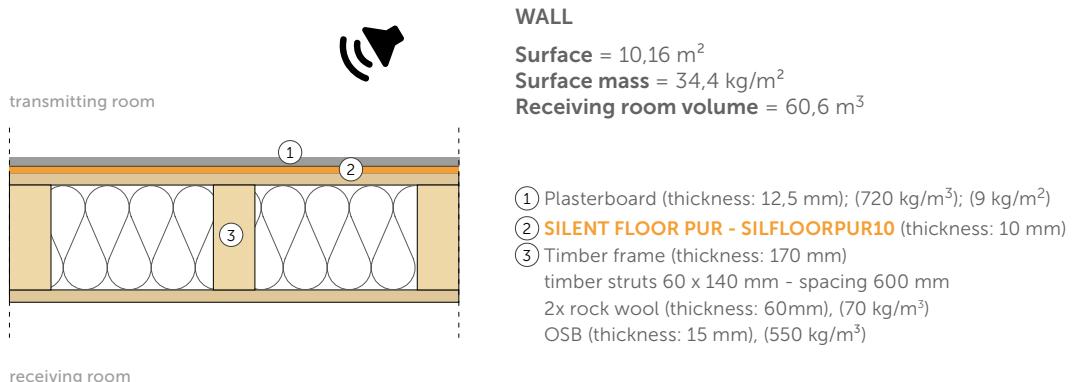
**Test protocol:** Pr. 2022-rothoLATE-R12b.

### NOTES:

<sup>(1)</sup> Increase due to the addition of layers no. 1 and no. 2.

## LABORATORY MEASUREMENT | FRAME WALL 7A

MEASUREMENT OF AIRBORNE SOUND INSULATION EVALUATION INDEX  
REFERENCE STANDARD: ISO 10140-2 AND EN ISO 717-1



## AIRBORNE SOUND INSULATION



$$R_w(C; C_{tr}) = 47 \text{ (-3;-9) dB}$$

$$STC = 47$$

$$\Delta R_w = +6 \text{ dB}^{(1)}$$

$$\Delta STC = +6 \text{ dB}^{(1)}$$

**Testing laboratory:** Building Physics Lab | Libera Università di Bolzano.

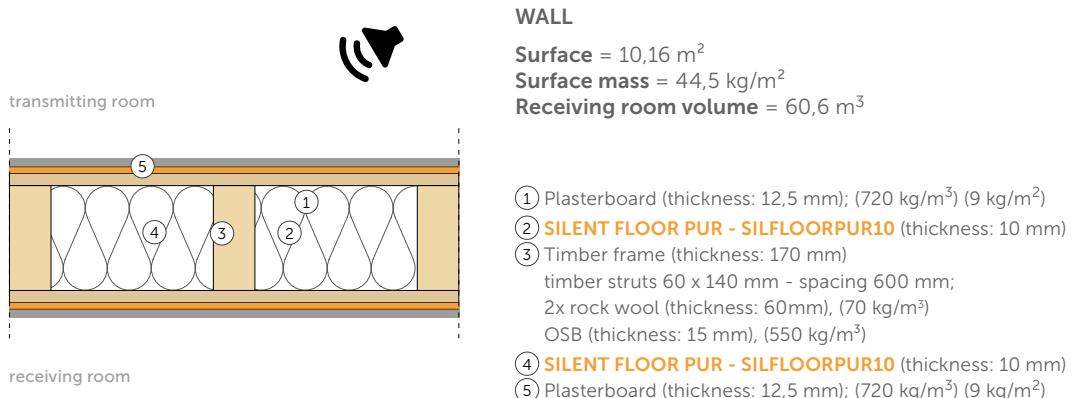
**Test protocol:** Pr. 2022-rothoLATE-R13a.

**NOTES:**

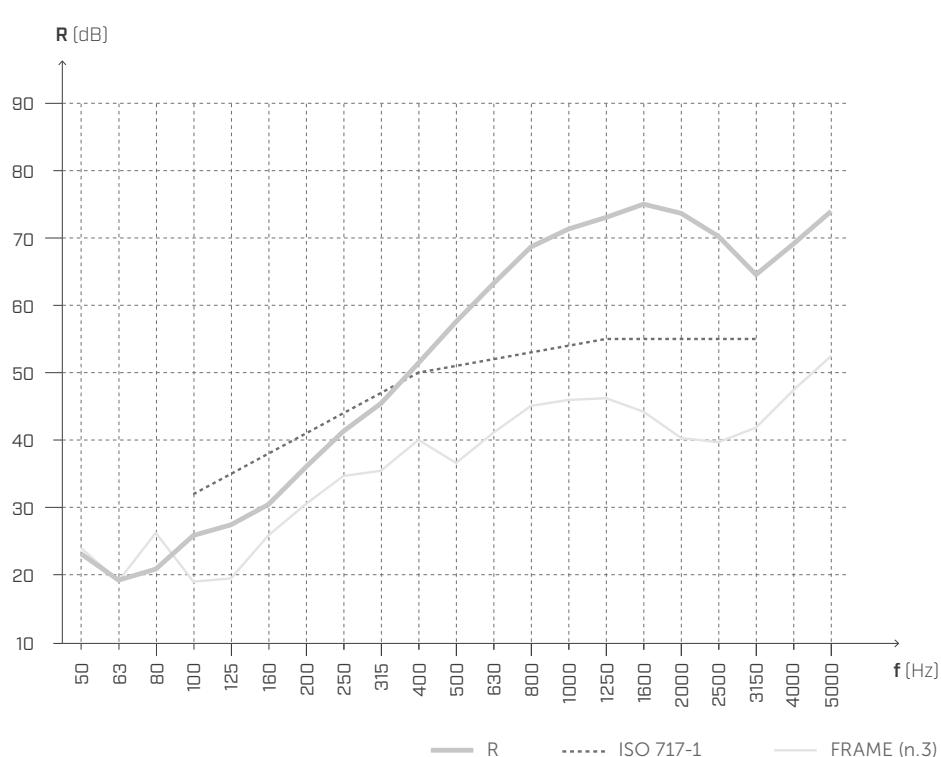
<sup>(1)</sup> Increase due to the addition of layers no. 1 and no. 2.

## LABORATORY MEASUREMENT | FRAME WALL 7B

MEASUREMENT OF AIRBORNE SOUND INSULATION EVALUATION INDEX  
REFERENCE STANDARD: ISO 10140-2 AND EN ISO 717-1



## AIRBORNE SOUND INSULATION



$$R_w(C, C_{tr}) = 51 \text{ (-3;-9) dB}$$

$$\Delta R_w = +10 \text{ dB}^{(1)}$$

$$STC = 51$$

$$\Delta STC = +10^{(1)}$$

Testing laboratory: Building Physics Lab | Libera Università di Bolzano.

Test protocol: Pr. 2022-rothoLATE-R13b.

### NOTES:

<sup>(1)</sup> Increase due to the addition of layers no. 1 and no. 2.

# ON SITE MEASUREMENTS

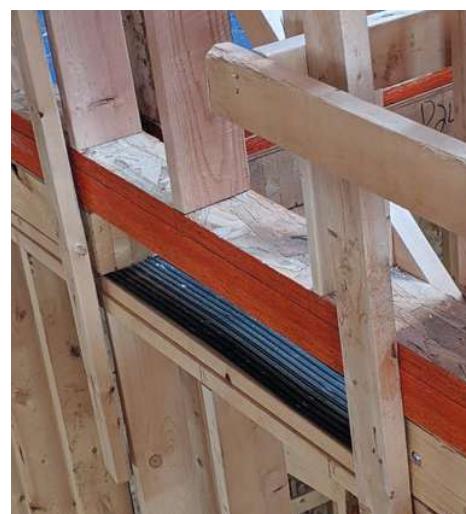
## COMMERCIAL BUILDING

Atlanta [USA]



The newly constructed building boasts office space, restaurants, shops, a hotel and art studios. It is a very innovative project that also uses TIMBER as a structural material. To improve the acoustic performance of the floors, SILENT FLOOR PUR was used and ALADIN was used to reduce lateral transmission.

<b>description</b>	commercial building covering more than 300000 sq ft
<b>type of structure</b>	mixed
<b>location</b>	Atlanta (Georgia, USA)
<b>products</b>	SILENT FLOOR PUR, ALADIN



# SILFLOORPUR15

## TECHNICAL DATA

Properties	standard	value
Surface mass m	-	1,4 kg/m <sup>2</sup>
Density ρ	-	90 kg/m <sup>3</sup>
Apparent dynamic stiffness s'	EN 29052-1	8,8 MN/m <sup>3</sup>
Dynamic stiffness s'	EN 29052-1	8,8 MN/m <sup>3</sup>
Theoretical estimate of impact sound pressure level attenuation ΔL <sub>w</sub> <sup>(1)</sup>	ISO 12354-2	34,6 dB
System resonance frequency f <sub>0</sub> <sup>(2)</sup>	ISO 12354-2	42,5 Hz
Impact sound pressure level attenuation ΔL <sub>w</sub> <sup>(3)</sup>	ISO 10140-3	23 dB
Thermal resistance R <sub>t</sub>	-	0,52 m <sup>2</sup> K/W
Resistance to airflow r	ISO 9053	< 10,0 kPa·s·m <sup>-2</sup>
Compressibility class	EN 12431	CP2
CREEP Viscous sliding under compression X <sub>ct</sub> (1,5 kPa)	EN 1606	7,50 %
Compression deformation stress	ISO 3386-1	17 kPa
Thermal conductivity λ	-	0,035 W/m·K
Specific heat c	-	1800 J/kg·K
Water vapour transmission S <sub>d</sub>	-	> 100 m
Reaction to fire	EN 13501-1	class F
VOC emission classification	French decree no. 2011-321	A+

<sup>(1)</sup>ΔL<sub>w</sub> = (13 lg(m')) - (14,2 lg(s')) + 20,8 [dB] con m' = 125 kg/m<sup>2</sup>.

<sup>(2)</sup>f<sub>0</sub> = 160 √(s'/m') con m' = 125 kg/m<sup>2</sup>.

<sup>(3)</sup>Measured in the laboratory on 200 mm CLT floor. See the manual for more information on configuration.

## EN ISO 12354-2 ANNEX C | ESTIMATE ΔL<sub>w</sub> [FORMULA C.4] E ΔL [FORMULA C.1]

The following tables show how the attenuation in dB (ΔL<sub>w</sub> e ΔL) of SILFLOORPUR15 varies as the load m' (i.e., the surface mass of the layers with which SILFLOORPUR15 is loaded) changes.

SILFLOORPUR15

s' or s'	8,8	8,8	8,8	8,8	8,8	8,8	8,8	8,8	8,8	8,8	[MN/m <sup>3</sup> ]
load m'	50	75	100	125	150	175	200	225	250	275	[kg/m <sup>2</sup> ]
ΔL <sub>w</sub>	29,5	31,8	33,4	34,6	35,7	36,5	37,3	38,0	38,6	39,1	[dB]
f <sub>0</sub>	67,1	54,8	47,5	42,5	38,8	35,9	33,6	31,6	30,0	28,6	[Hz]

ΔL in frequency

[Hz]	<b>100</b>	5,2	7,8	9,7	11,2	12,4	13,4	14,2	15,0	15,7	16,3	16,9	[dB]
[Hz]	<b>125</b>	8,1	10,7	12,6	14,1	15,3	16,3	17,1	17,9	18,6	19,2	19,8	[dB]
[Hz]	<b>160</b>	11,3	14,0	15,8	17,3	18,5	19,5	20,3	21,1	21,8	22,4	23,0	[dB]
[Hz]	<b>200</b>	14,2	16,9	18,7	20,2	21,4	22,4	23,3	24,0	24,7	25,3	25,9	[dB]
[Hz]	<b>250</b>	17,1	19,8	21,6	23,1	24,3	25,3	26,2	26,9	27,6	28,2	28,8	[dB]
[Hz]	<b>315</b>	20,1	22,8	24,7	26,1	27,3	28,3	29,2	29,9	30,6	31,2	31,8	[dB]
[Hz]	<b>400</b>	23,3	25,9	27,8	29,2	30,4	31,4	32,3	33,1	33,7	34,4	34,9	[dB]
[Hz]	<b>500</b>	26,2	28,8	30,7	32,1	33,3	34,3	35,2	36,0	36,6	37,3	37,8	[dB]
[Hz]	<b>630</b>	29,2	31,8	33,7	35,1	36,3	37,3	38,2	39,0	39,7	40,3	40,8	[dB]
[Hz]	<b>800</b>	32,3	34,9	36,8	38,3	39,4	40,4	41,3	42,1	42,8	43,4	44,0	[dB]
[Hz]	<b>1000</b>	35,2	37,8	39,7	41,2	42,4	43,4	44,2	45,0	45,7	46,3	46,9	[dB]
[Hz]	<b>1250</b>	38,1	40,7	42,6	44,1	45,3	46,3	47,1	47,9	48,6	49,2	49,8	[dB]
[Hz]	<b>1600</b>	41,3	44,0	45,8	47,3	48,5	49,5	50,3	51,1	51,8	52,4	53,0	[dB]
[Hz]	<b>2000</b>	44,2	46,9	48,7	50,2	51,4	52,4	53,3	54,0	54,7	55,3	55,9	[dB]
[Hz]	<b>2500</b>	47,1	49,8	51,6	53,1	54,3	55,3	56,2	56,9	57,6	58,2	58,8	[dB]
[Hz]	<b>3150</b>	50,1	52,8	54,7	56,1	57,3	58,3	59,2	59,9	60,6	61,2	61,8	[dB]

EN ISO 12354-2 Annex C - formula C.4

EN ISO 12354-2 Annex C - formula C.1

$$\square \quad \Delta L_w = \left( 13 \lg(m') \right) - \left( 14,2 \lg(s') \right) + 20,8 \text{ dB}$$

$$\square \quad \Delta L = \left( 30 \lg \frac{f}{f_0} \right) \text{ dB}$$

EN ISO 12354-2 Annex C - formula C.2

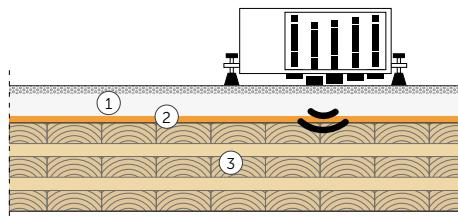
$$\square \quad f_0 = 160 \sqrt{\frac{s'}{m'}}$$

## LABORATORY MEASUREMENT | CLT FLOOR 1

MEASUREMENT OF THE EVALUATION INDEX OF THE REDUCTION OF THE IMPACT SOUND PRESSURE LEVEL  
REFERENCE STANDARD: ISO 10140-3 AND EN ISO 717-2

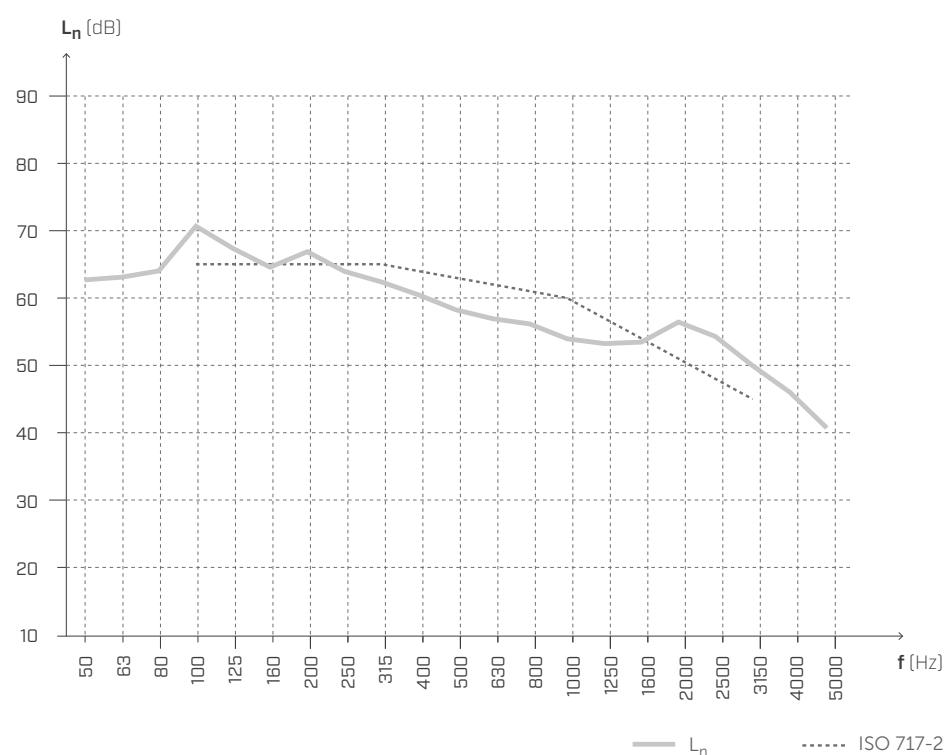
### FLOOR SLAB

Surface = 13,71 m<sup>2</sup>  
Surface mass = 215,7 kg/m<sup>2</sup>  
Receiving room volume = 60,1 m<sup>3</sup>



- ① Concrete screed (thickness: 50 mm); (2600 kg/m<sup>3</sup>); (130 kg/m<sup>2</sup>)
- ② **SILENT FLOOR PUR - SILFLOORPUR15** (thickness: 15 mm)
- ③ CLT 5 layers (thickness: 200 mm); (420 kg/m<sup>3</sup>); (84 kg/m<sup>2</sup>)

## IMPACT SOUND INSULATION



$$L_{n,w}(C_1) = \text{63 (-3) dB}$$

$$\Delta L_{n,w} = -23 \text{ dB}^{(1)}$$

$$\text{IIC} = \text{47}$$

$$\Delta \text{IIC} = +23^{(2)}$$

Testing laboratory: Building Physics Lab | Libera Università di Bolzano.

Test protocol: Pr. 2022-rothoLATE-L6.

### NOTES:

<sup>(1)</sup> Decrease due to the addition of layers no. 1 and no. 2.

<sup>(2)</sup> Increase due to the addition of layers no. 1 and no. 2.

## ■ LABORATORY MEASUREMENT | CLT FLOOR 1

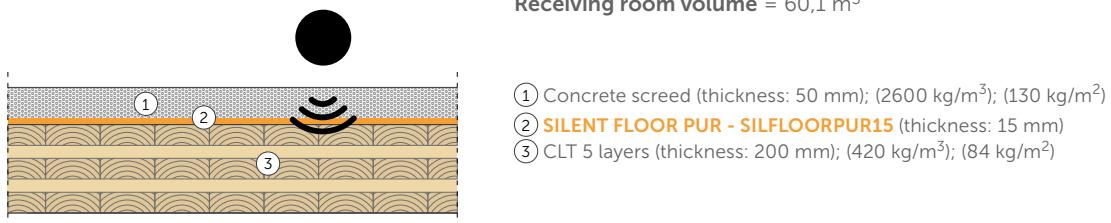
MEASUREMENT OF THE EVALUATION INDEX OF THE REDUCTION OF THE IMPACT SOUND PRESSURE LEVEL  
RUBBER BALL METHOD | REFERENCE STANDARD: ISO 16283-2

### FLOOR SLAB

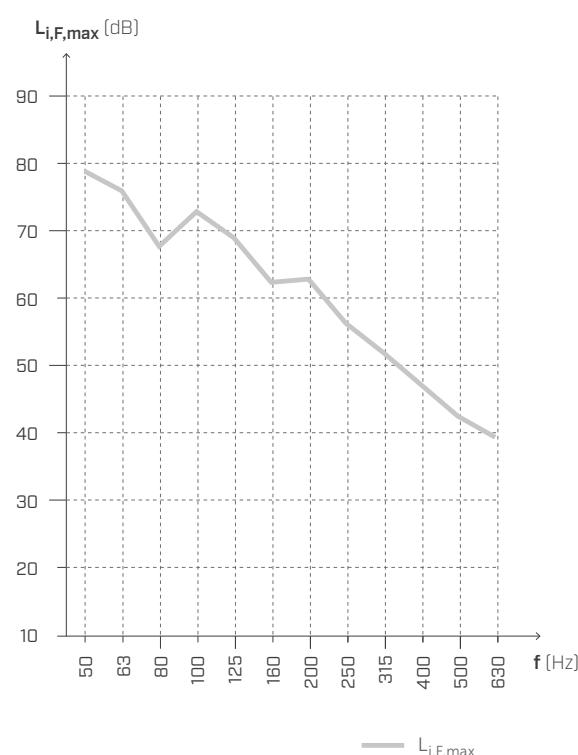
Surface = 13,71 m<sup>2</sup>

Surface mass = 215,7 kg/m<sup>2</sup>

Receiving room volume = 60,1 m<sup>3</sup>



## ■ IMPACT SOUND INSULATION



f [Hz]	$L_{i,F,\max}$ [dB]
50	78,8
63	75,9
80	67,7
100	72,8
125	68,9
160	62,3
200	62,8
250	56,3
315	51,9
400	47,2
500	42,5
630	39,4

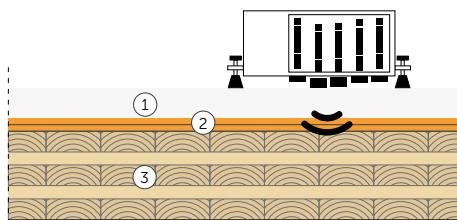
Testing laboratory: Building Physics Lab | Libera Università di Bolzano.  
Test protocol: Pr. 2022-rothoLATE-L6.

## LABORATORY MEASUREMENT | CLT FLOOR 2

MEASUREMENT OF THE EVALUATION INDEX OF THE REDUCTION OF THE IMPACT SOUND PRESSURE LEVEL  
REFERENCE STANDARD: ISO 10140-3 AND EN ISO 717-2

### FLOOR SLAB

Surface = 13,71 m<sup>2</sup>  
Surface mass = 217,3 kg/m<sup>2</sup>  
Receiving room volume = 60,1 m<sup>3</sup>



- ① Concrete screed (thickness: 50 mm); (2600 kg/m<sup>3</sup>); (130 kg/m<sup>2</sup>)
- ② 2x SILENT FLOOR PUR - SILFLOORPUR15 (thickness: 15 mm)
- ③ CLT 5 layers (thickness: 200 mm); (420 kg/m<sup>3</sup>); (84 kg/m<sup>2</sup>)

## IMPACT SOUND INSULATION



$$L_{n,w}(C_l) = \mathbf{60 \, (-4) \, dB}$$

$$\Delta L_{n,w} = -26 \, dB^{(1)}$$

$$IIC = \mathbf{50}$$

$$\Delta IIC = +26^{(2)}$$

Testing laboratory: Building Physics Lab | Libera Università di Bolzano.

Test protocol: Pr. 2022-rothoLATE-L6.

### NOTES:

<sup>(1)</sup> Decrease due to the addition of layers no. 1 and no. 2.

<sup>(2)</sup> Increase due to the addition of layers no. 1 and no. 2.

## ■ LABORATORY MEASUREMENT | CLT FLOOR 2

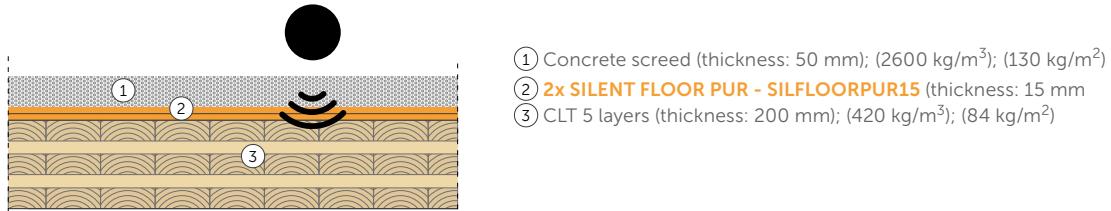
MEASUREMENT OF THE EVALUATION INDEX OF THE REDUCTION OF THE IMPACT SOUND PRESSURE LEVEL  
RUBBER BALL METHOD | REFERENCE STANDARD: ISO 16283-2

### FLOOR SLAB

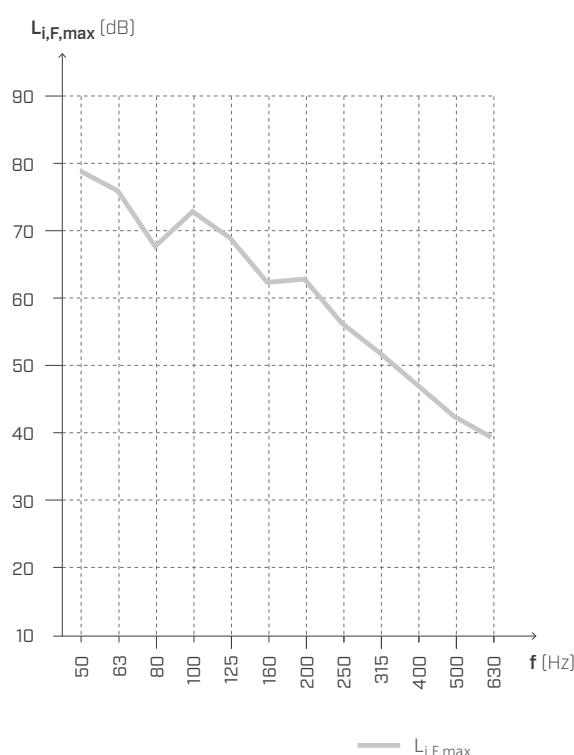
Surface = 13,71 m<sup>2</sup>

Surface mass = 217,3 kg/m<sup>2</sup>

Receiving room volume = 60,1 m<sup>3</sup>



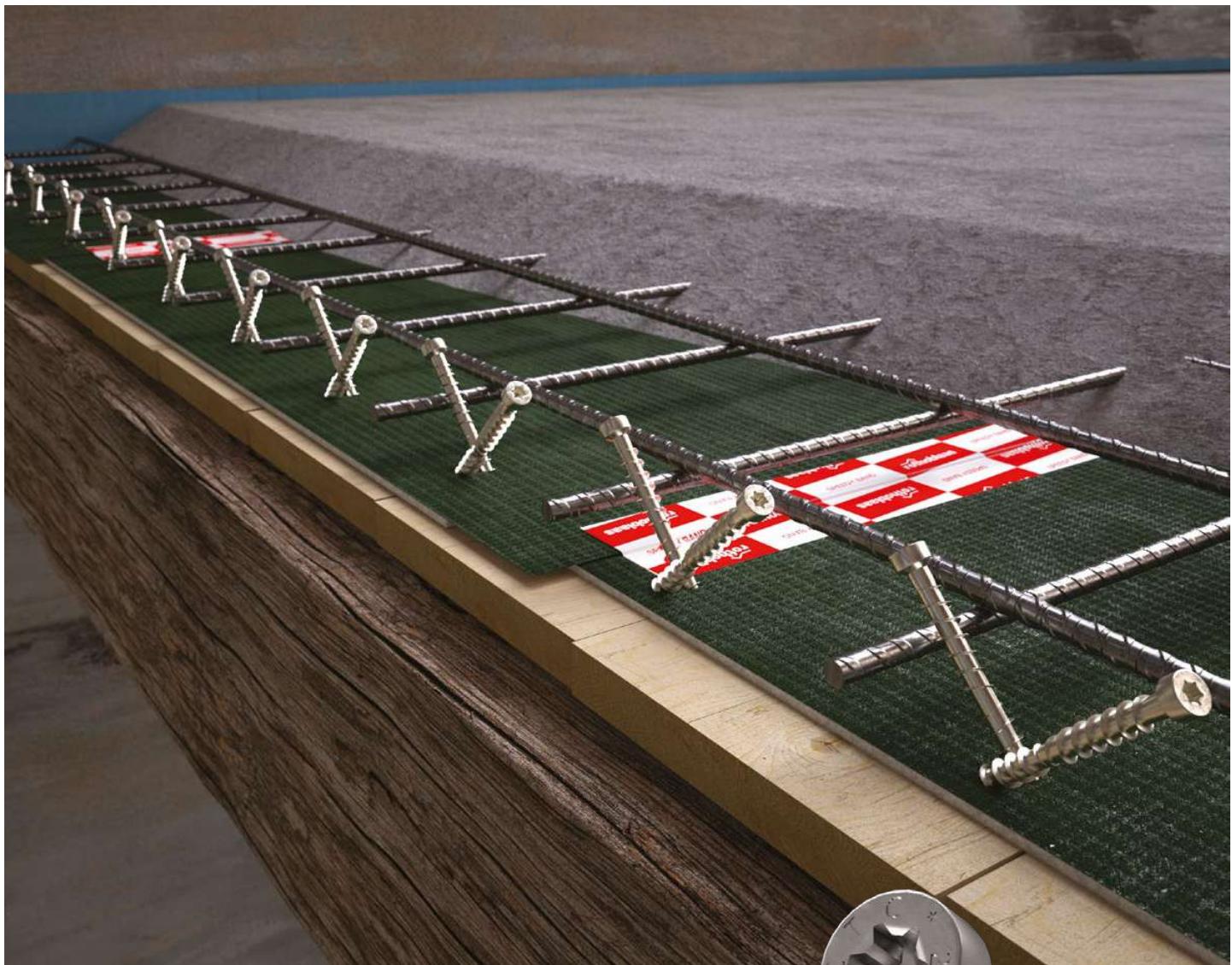
## ■ IMPACT SOUND INSULATION



f [Hz]	$L_{i,F,\max}$ [dB]
50	81,5
63	79,0
80	68,2
100	65,2
125	63,5
160	57,8
200	59,6
250	52,9
315	48,5
400	44,3
500	40,7
630	38,0

Testing laboratory: Building Physics Lab | Libera Università di Bolzano.  
Test protocol: Pr. 2022-rothoLATE-L6.

# CERTAIN COLLABORATIONS ARE BORN TO LAST



CTC is the connector for timber-to-concrete floors.

CE certified, it allows to connect a 5 or 6 cm reinforced concrete slab to the timber beams of the underneath floor, obtaining a new timber-concrete structure with extraordinary strength and excellent static and acoustic performance. It is an approved self-drilling, reversible, fast and minimally invasive system.



Scan the QR code and discover the technical features of CTC connector



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Solutions for Building Technology

# SILFLOORPUR20

## TECHNICAL DATA

Properties	standard	value
Surface mass m	-	1,8 kg/m <sup>2</sup>
Density ρ	-	90 kg/m <sup>3</sup>
Apparent dynamic stiffness s'	EN 29052-1	7,4 MN/m <sup>3</sup>
Dynamic stiffness s'	EN 29052-1	7,4 MN/m <sup>3</sup>
Theoretical estimate of impact sound pressure level attenuation ΔL <sub>w</sub> <sup>(1)</sup>	ISO 12354-2	35,7 dB
System resonance frequency f <sub>0</sub> <sup>(2)</sup>	ISO 12354-2	38,9 Hz
Impact sound pressure level attenuation ΔL <sub>w</sub> <sup>(3)</sup>	ISO 10140-3	25 dB
Thermal resistance R <sub>t</sub>	-	0,92 m <sup>2</sup> K/W
Resistance to airflow r	ISO 9053	< 10,0 kPa·s·m <sup>-2</sup>
Compressibility class	EN 12431	CP2
CREEP Viscous sliding under compression X <sub>ct</sub> (1,5 kPa)	EN 1606	7,50 %
Compression deformation stress	ISO 3386-1	17 kPa
Thermal conductivity λ	-	0,035 W/m·K
Specific heat c	-	1800 J/kg·K
Water vapour transmission S <sub>d</sub>	-	> 100 m
Reaction to fire	EN 13501-1	class F
VOC emission classification	French decree no. 2011-321	A+

<sup>(1)</sup>ΔL<sub>w</sub> = (13 lg(m')) - (14,2 lg(s')) + 20,8 [dB] con m' = 125 kg/m<sup>2</sup>.

<sup>(2)</sup>f<sub>0</sub> = 160 √(s'/m') con m' = 125 kg/m<sup>2</sup>.

<sup>(3)</sup>Measured in the laboratory on 200 mm CLT floor. See the manual for more information on configuration.

## EN ISO 12354-2 ANNEX C | ESTIMATE ΔL<sub>w</sub> [FORMULA C.4] E ΔL [FORMULA C.1]

The following tables show how the attenuation in dB (ΔL<sub>w</sub> e ΔL) of SILFLOORPUR20 varies as the load m' (i.e., the surface mass of the layers with which SILFLOORPUR20 is loaded) changes.

SILFLOORPUR20

s' or s'	12,5	12,5	12,5	12,5	12,5	12,5	12,5	12,5	12,5	12,5	[MN/m <sup>3</sup> ]
load m'	50	75	100	125	150	175	200	225	250	275	[kg/m <sup>2</sup> ]
ΔL <sub>w</sub>	27,3	29,6	31,2	32,5	33,5	34,4	35,1	35,8	36,4	36,9	[dB]
f <sub>0</sub>	80,0	65,3	56,6	50,6	46,2	42,8	40,0	37,7	35,8	34,1	[Hz]

ΔL in frequency

[Hz]	<b>100</b>	2,9	5,5	7,4	8,9	10,1	11,1	11,9	12,7	13,4	14,0	14,6	[dB]
[Hz]	<b>125</b>	5,8	8,5	10,3	11,8	13,0	14,0	14,8	15,6	16,3	16,9	17,5	[dB]
[Hz]	<b>160</b>	9,0	11,7	13,5	15,0	16,2	17,2	18,1	18,8	19,5	20,1	20,7	[dB]
[Hz]	<b>200</b>	11,9	14,6	16,5	17,9	19,1	20,1	21,0	21,7	22,4	23,0	23,6	[dB]
[Hz]	<b>250</b>	14,8	17,5	19,4	20,8	22,0	23,0	23,9	24,6	25,3	26,0	26,5	[dB]
[Hz]	<b>315</b>	17,9	20,5	22,4	23,8	25,0	26,0	26,9	27,7	28,3	29,0	29,5	[dB]
[Hz]	<b>400</b>	21,0	23,6	25,5	26,9	28,1	29,1	30,0	30,8	31,5	32,1	32,6	[dB]
[Hz]	<b>500</b>	23,9	26,5	28,4	29,8	31,0	32,0	32,9	33,7	34,4	35,0	35,5	[dB]
[Hz]	<b>630</b>	26,9	29,5	31,4	32,9	34,0	35,0	35,9	36,7	37,4	38,0	38,6	[dB]
[Hz]	<b>800</b>	30,0	32,6	34,5	36,0	37,2	38,2	39,0	39,8	40,5	41,1	41,7	[dB]
[Hz]	<b>1000</b>	32,9	35,5	37,4	38,9	40,1	41,1	41,9	42,7	43,4	44,0	44,6	[dB]
[Hz]	<b>1250</b>	35,8	38,5	40,3	41,8	43,0	44,0	44,8	45,6	46,3	46,9	47,5	[dB]
[Hz]	<b>1600</b>	39,0	41,7	43,5	45,0	46,2	47,2	48,1	48,8	49,5	50,1	50,7	[dB]
[Hz]	<b>2000</b>	41,9	44,6	46,5	47,9	49,1	50,1	51,0	51,7	52,4	53,0	53,6	[dB]
[Hz]	<b>2500</b>	44,8	47,5	49,4	50,8	52,0	53,0	53,9	54,6	55,3	56,0	56,5	[dB]
[Hz]	<b>3150</b>	47,9	50,5	52,4	53,8	55,0	56,0	56,9	57,7	58,3	59,0	59,5	[dB]

EN ISO 12354-2 Annex C - formula C.4

EN ISO 12354-2 Annex C - formula C.1

$$\square \quad \Delta L_w = \left( 13 \lg(m') \right) - \left( 14,2 \lg(s') \right) + 20,8 \text{ dB}$$

$$\square \quad \Delta L = \left( 30 \lg \frac{f}{f_0} \right) \text{dB}$$

EN ISO 12354-2 Annex C - formula C.2

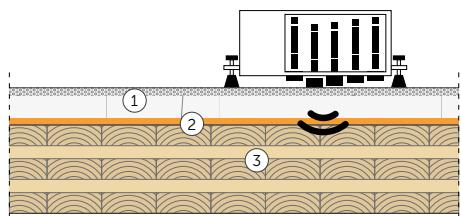
$$\square \quad f_0 = 160 \sqrt{\frac{s'}{m'}}$$

## LABORATORY MEASUREMENT | CLT FLOOR 1

MEASUREMENT OF THE EVALUATION INDEX OF THE REDUCTION OF THE IMPACT SOUND PRESSURE LEVEL  
REFERENCE STANDARD: ISO 10140-3 AND EN ISO 717-2

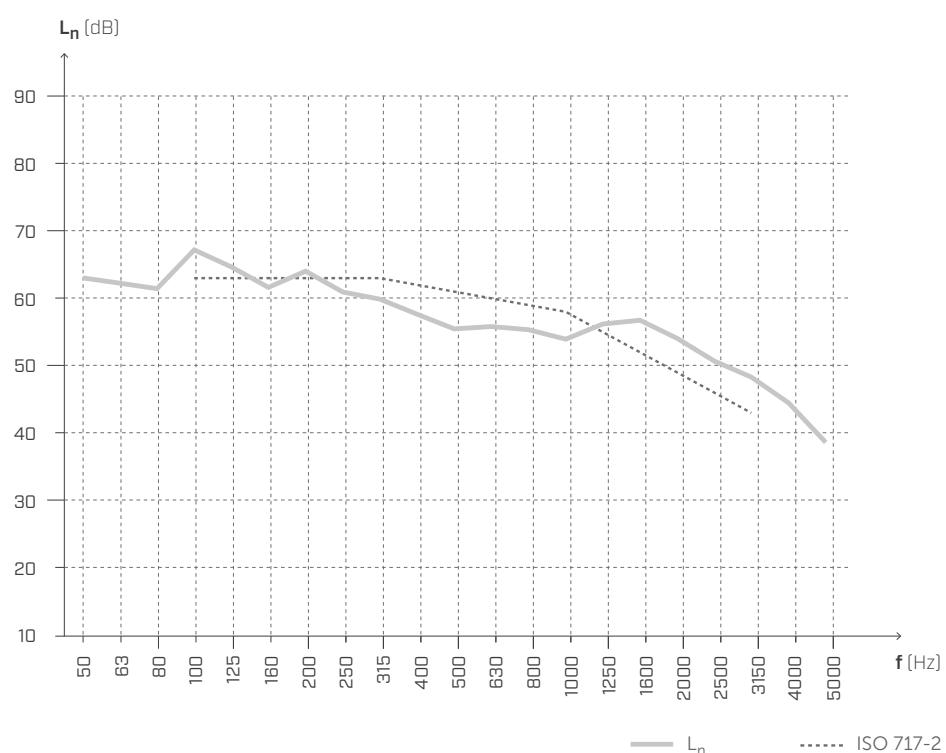
### FLOOR SLAB

**Surface** = 13,71 m<sup>2</sup>  
**Surface mass** = 216,2 kg/m<sup>2</sup>  
**Receiving room volume** = 60,1 m<sup>3</sup>



- ① Concrete screed (thickness: 50 mm); (2600 kg/m<sup>3</sup>); (130 kg/m<sup>2</sup>)
- ② **SILENT FLOOR PUR - SILFLOORPUR20** (thickness: 20 mm)
- ③ CLT 5 layers (thickness: 200 mm); (420 kg/m<sup>3</sup>); (84 kg/m<sup>2</sup>)

## IMPACT SOUND INSULATION



$$L_{n,w}(C_l) = \text{61 (-4) dB}$$

$$\Delta L_{n,w} = -25 \text{ dB}^{(1)}$$

$$IIC = 49$$

$$\Delta IIC = +25^{(2)}$$

**Testing laboratory:** Building Physics Lab | Libera Università di Bolzano.

**Test protocol:** Pr. 2022-rothoLATE-L1.

### NOTES:

<sup>(1)</sup> Decrease due to the addition of layers no. 1 and no. 2.

<sup>(2)</sup> Increase due to the addition of layers no. 1 and no. 2.

## ■ LABORATORY MEASUREMENT | CLT FLOOR 1

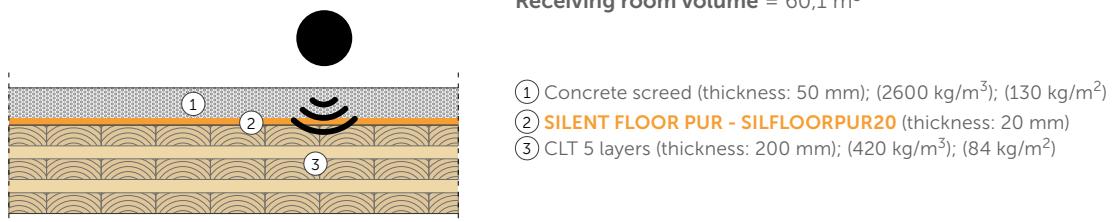
MEASUREMENT OF THE EVALUATION INDEX OF THE REDUCTION OF THE IMPACT SOUND PRESSURE LEVEL  
RUBBER BALL METHOD | REFERENCE STANDARD: ISO 16283-2

### FLOOR SLAB

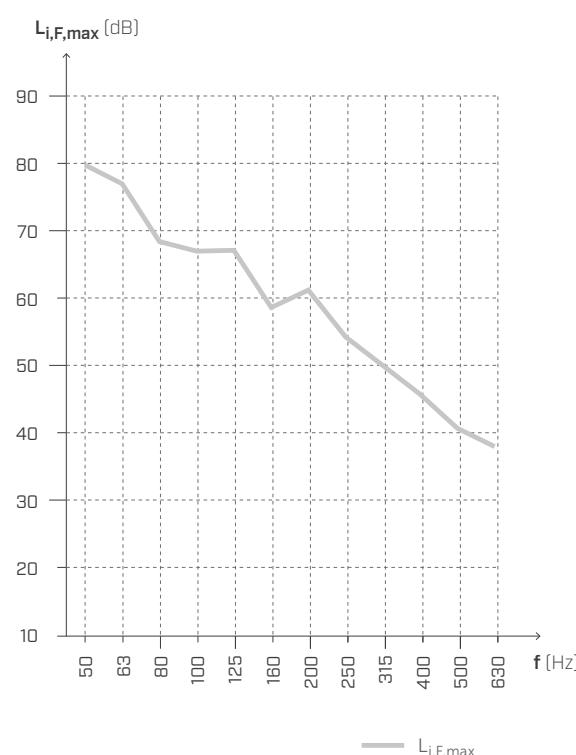
Surface = 13,71 m<sup>2</sup>

Surface mass = 216,2 kg/m<sup>2</sup>

Receiving room volume = 60,1 m<sup>3</sup>



## ■ IMPACT SOUND INSULATION



$f$ [Hz]	$L_{i,F,\max}$ [dB]
50	79,8
63	77,0
80	68,4
100	67,0
125	67,1
160	58,6
200	61,2
250	54,2
315	50,0
400	45,7
500	40,7
630	38,0

Testing laboratory: Building Physics Lab | Libera Università di Bolzano.  
Test protocol: Pr. 2022-rothoLATE-L1.

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